

# Model Predictive Control in Medium-Voltage Drives

Tobias Geyer



Department of Electrical and Computer Engineering  
The University of Auckland  
New Zealand

In collaboration with



# Outline

---

## Introduction

- Control problem
- Performance trade-off
- Control and modulation schemes

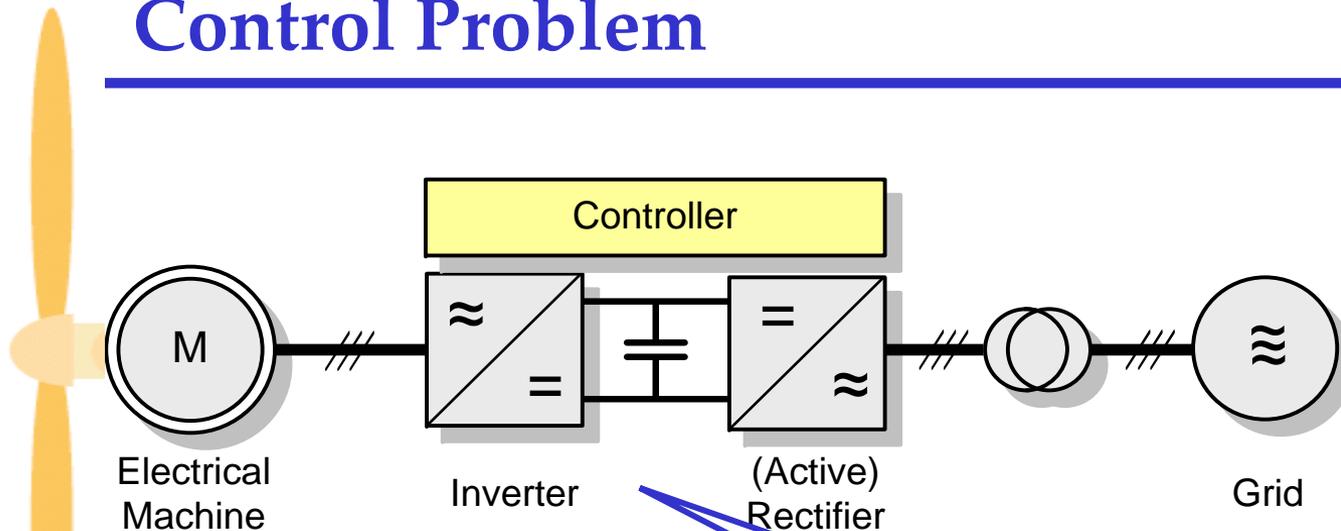
## Model Predictive Control

- 1-step predictive control
- Model predictive direct current/torque control
- Computational efficiency

## Summary and Outlook

# Control Problem

# Control Problem



Low **current** distortions  
=> low **thermal** losses

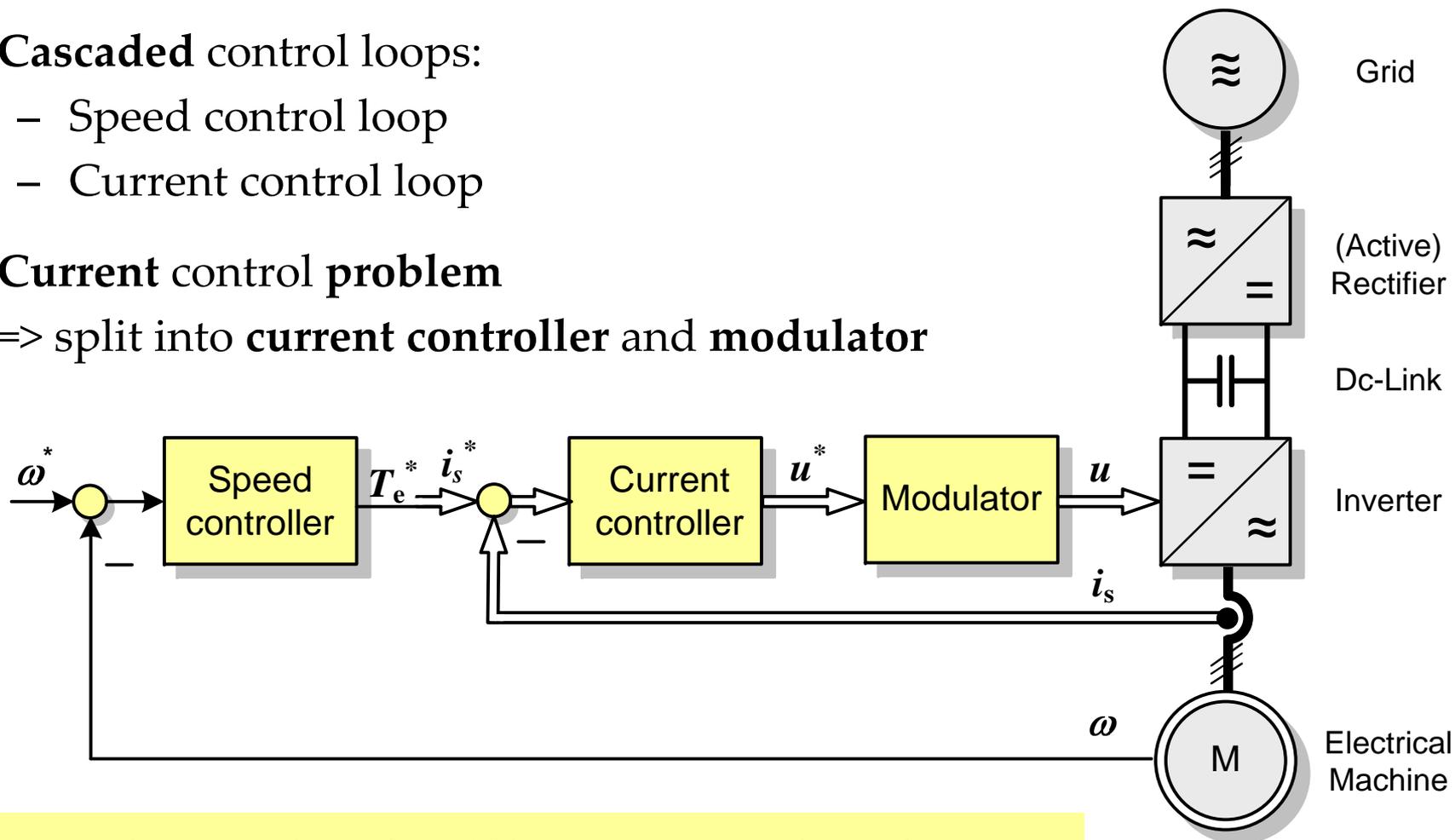
Low **torque** distortions => no  
excitation of mech. **resonances**

**Fast** torque response => high  
**dynamic** performance

Low switching **losses** => high  
**efficiency**, low **thermal** losses

# Control and Modulation

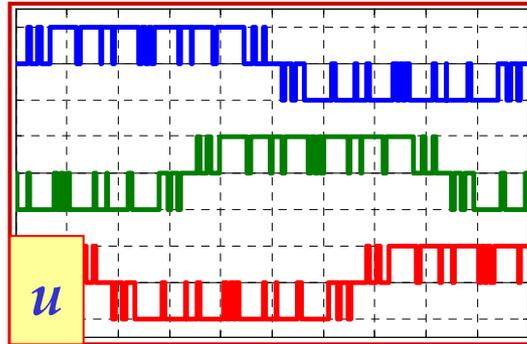
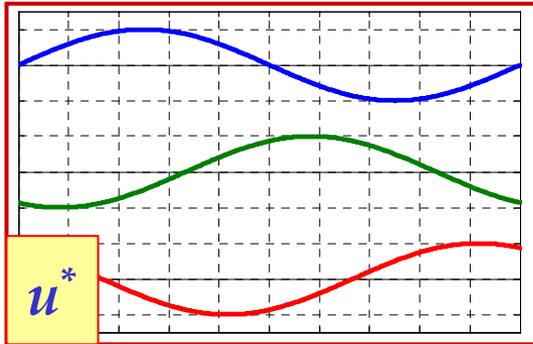
- **Cascaded** control loops:
  - Speed control loop
  - Current control loop
- **Current control problem**  
=> split into **current controller** and **modulator**



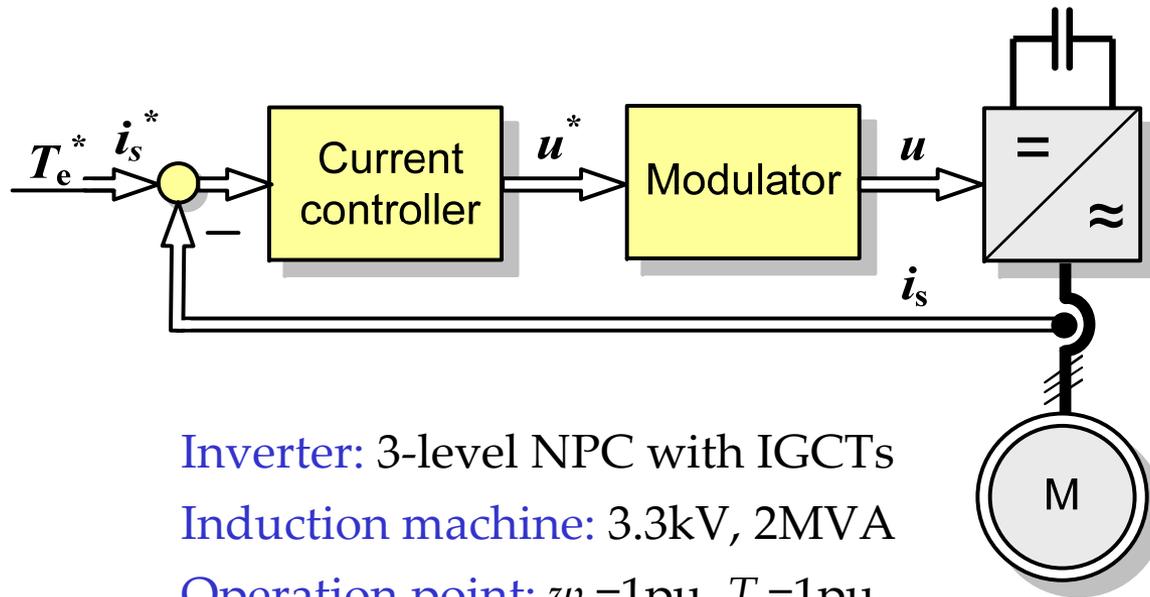
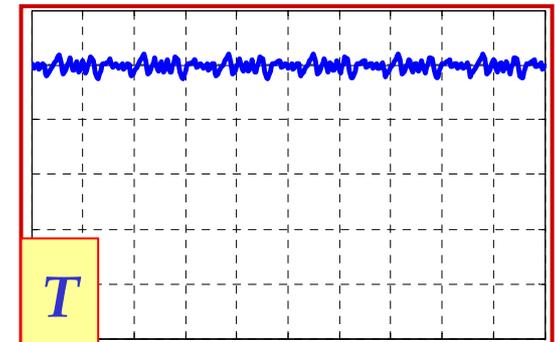
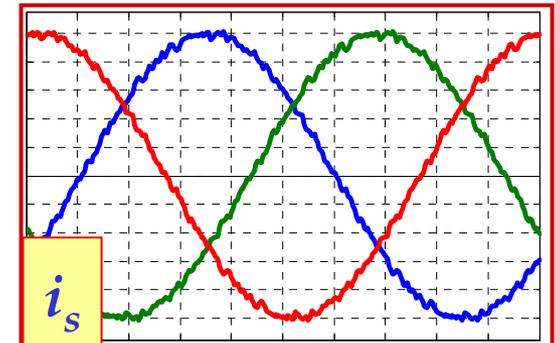
Fundamental **trade-off** between switching losses (frequency) and the current / torque **distortion** levels

# Performance Trade-Off

# Trade-Off (*High Switching Frequency*)

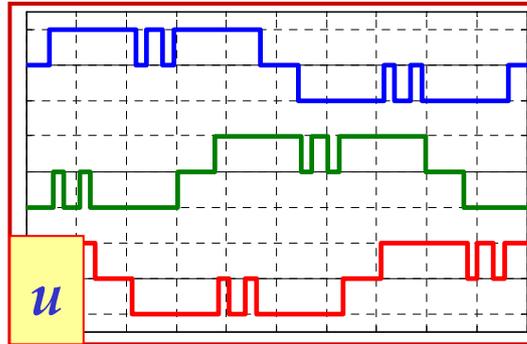
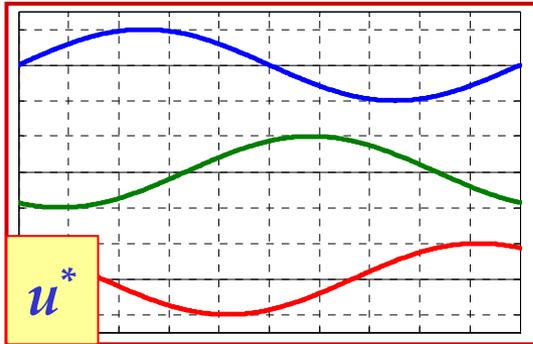


$f_{sw} = 700\text{Hz}$   
 $P_{sw} = 16.7\text{kW}, P_{con} = 2.7\text{kW}$   
 $\text{THD}_I = 2.31\%$   
 $\text{THD}_T = 1.93\%$

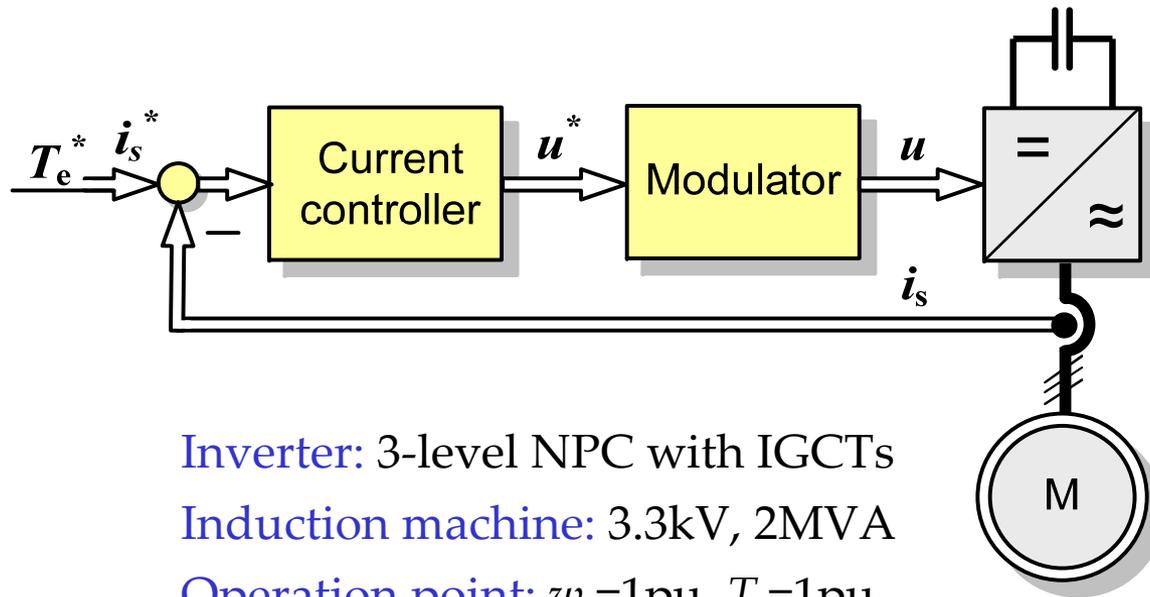


Inverter: 3-level NPC with IGCTs  
 Induction machine: 3.3kV, 2MVA  
 Operation point:  $w_e = 1\text{pu}, T_e = 1\text{pu}$

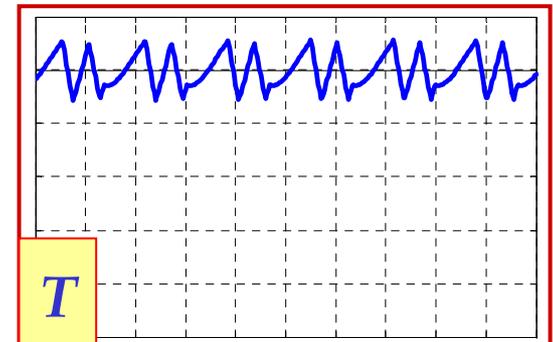
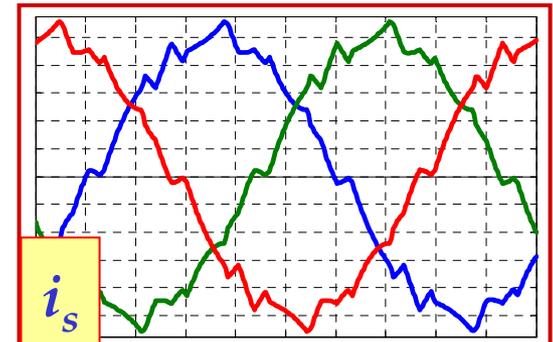
# Trade-Off (*Low* Switching Frequency)



$f_{sw} = 150\text{Hz}$   
 $P_{sw} = 3.9\text{kW}, P_{con} = 2.8\text{kW}$   
 $\text{THD}_I = 6.9\%$   
 $\text{THD}_T = 6.0\%$

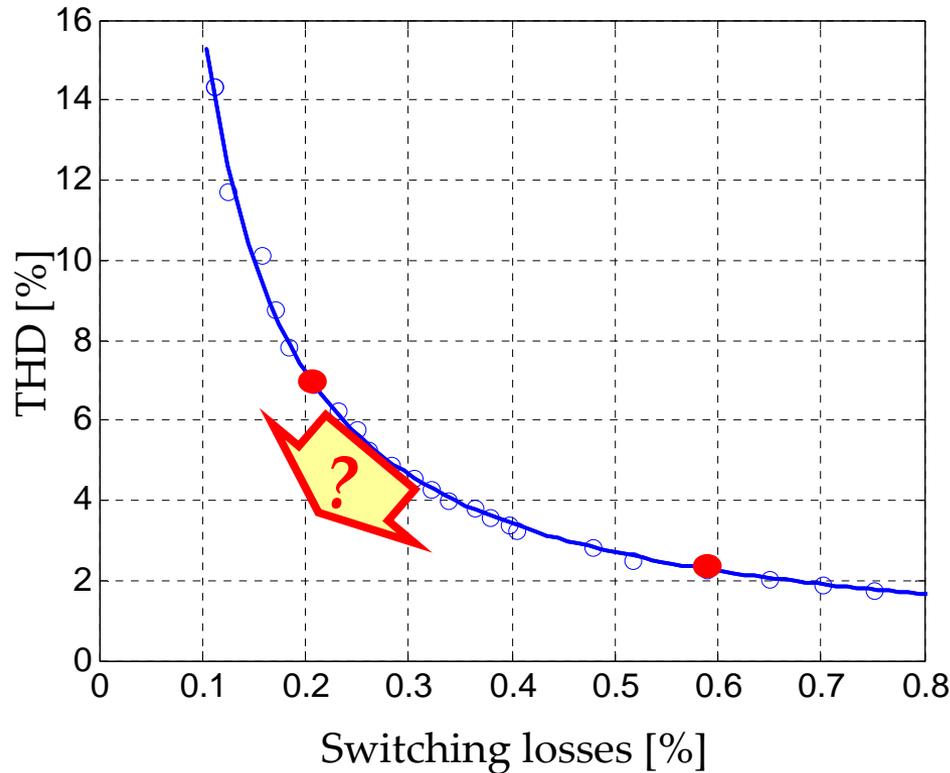


Inverter: 3-level NPC with IGCTs  
 Induction machine: 3.3kV, 2MVA  
 Operation point:  $w_e = 1\text{pu}, T_e = 1\text{pu}$



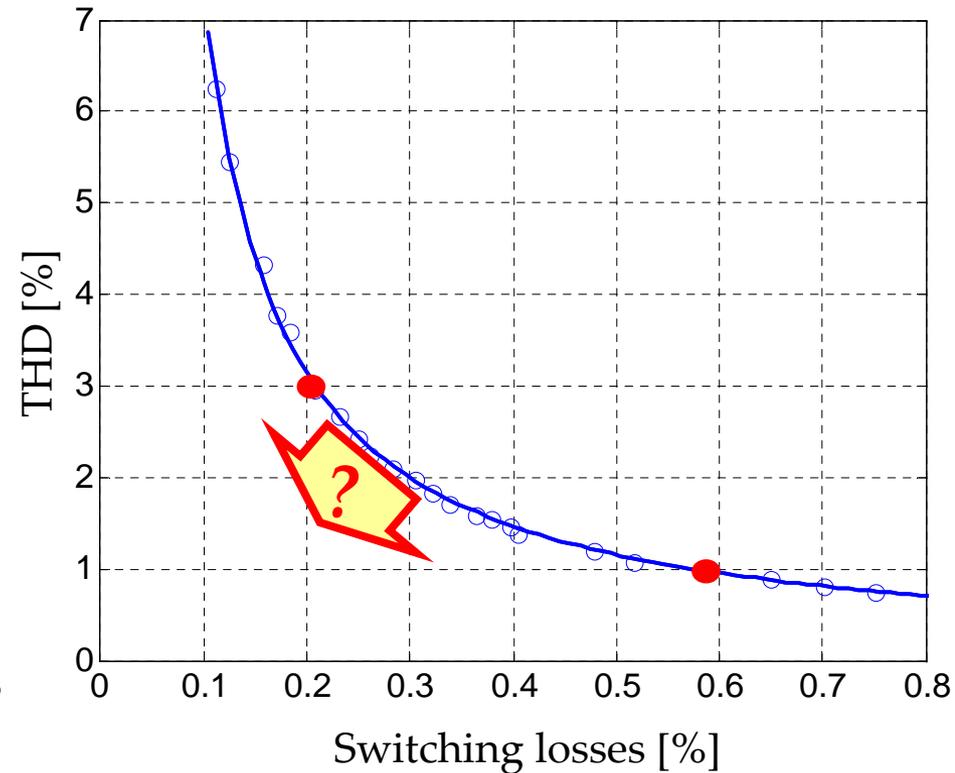
# Trade-Off for PWM / SVM

## Current THD vs switching losses



$$I_{s,THD} \cdot P_{sw} = \text{const}$$

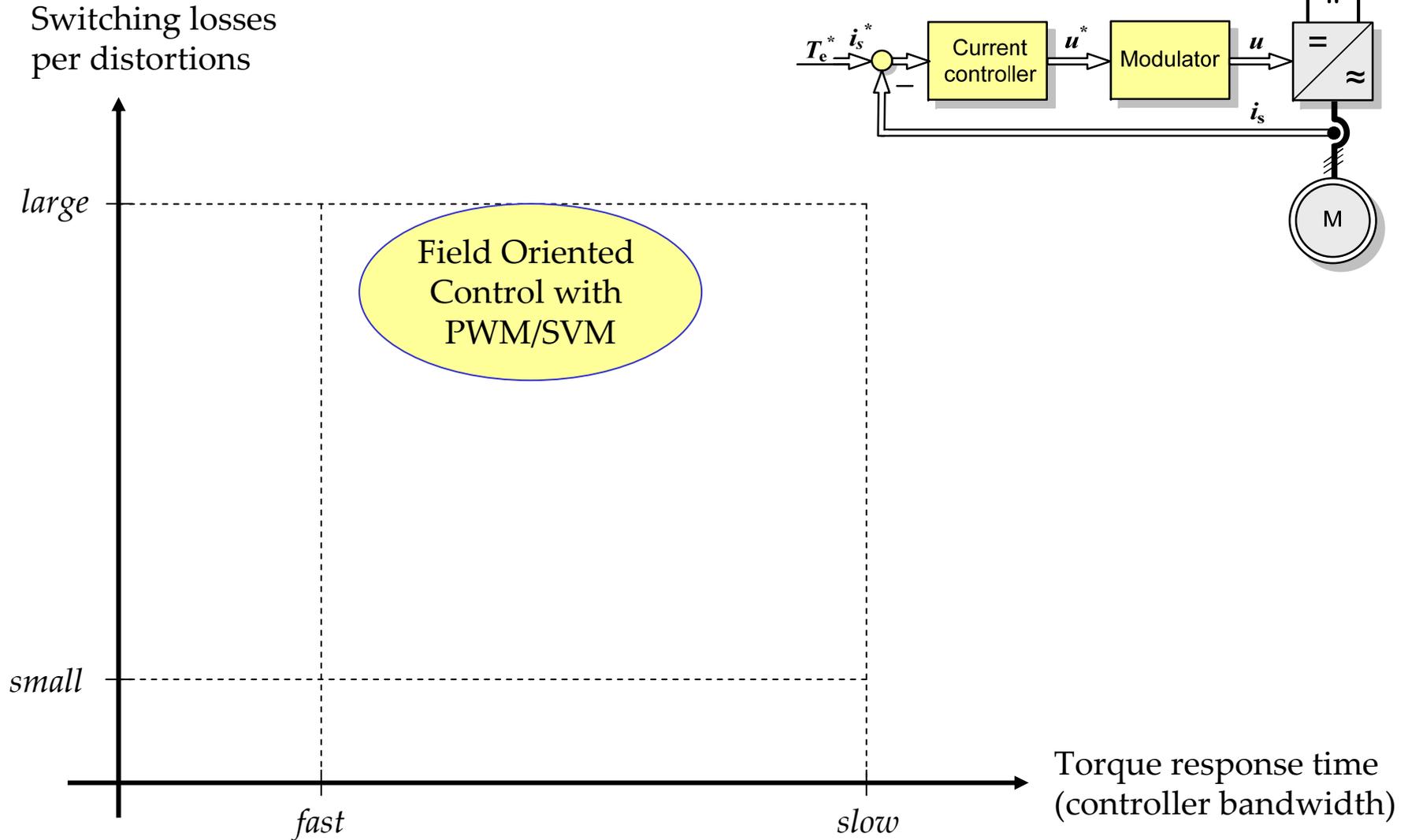
## Torque THD vs switching losses



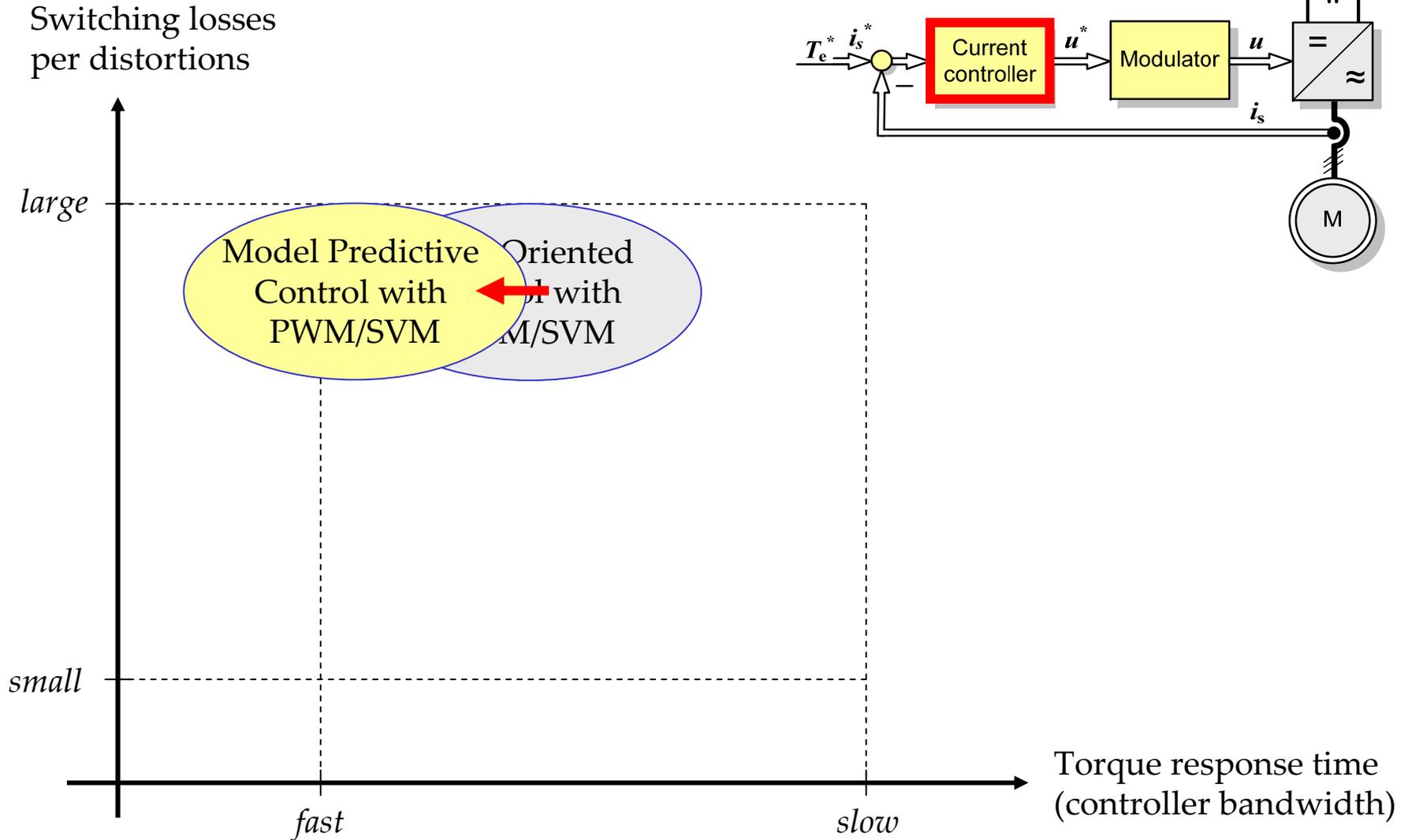
$$T_{e,THD} \cdot P_{sw} = \text{const}$$

# Control and Modulation Schemes

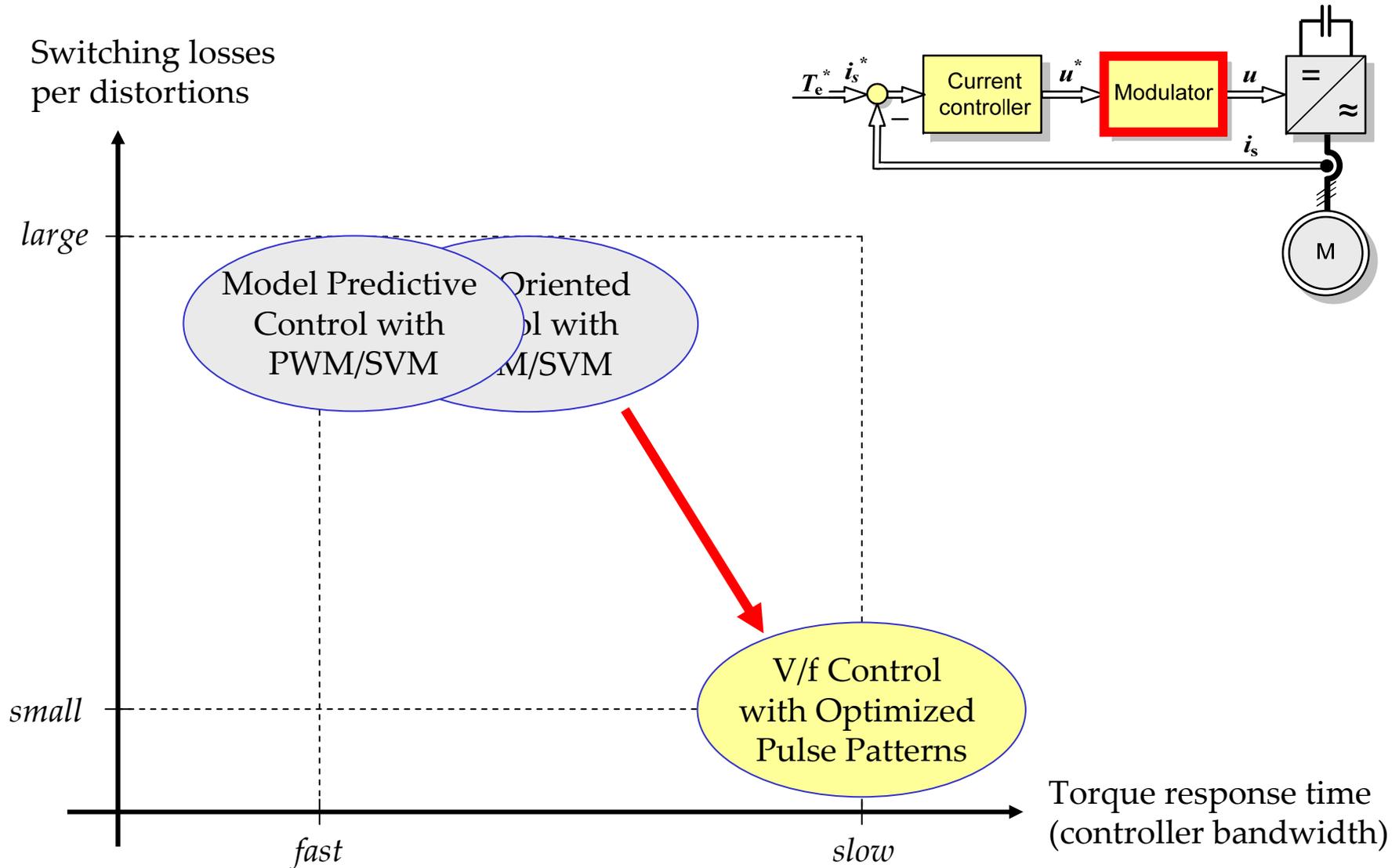
# Control and Modulation



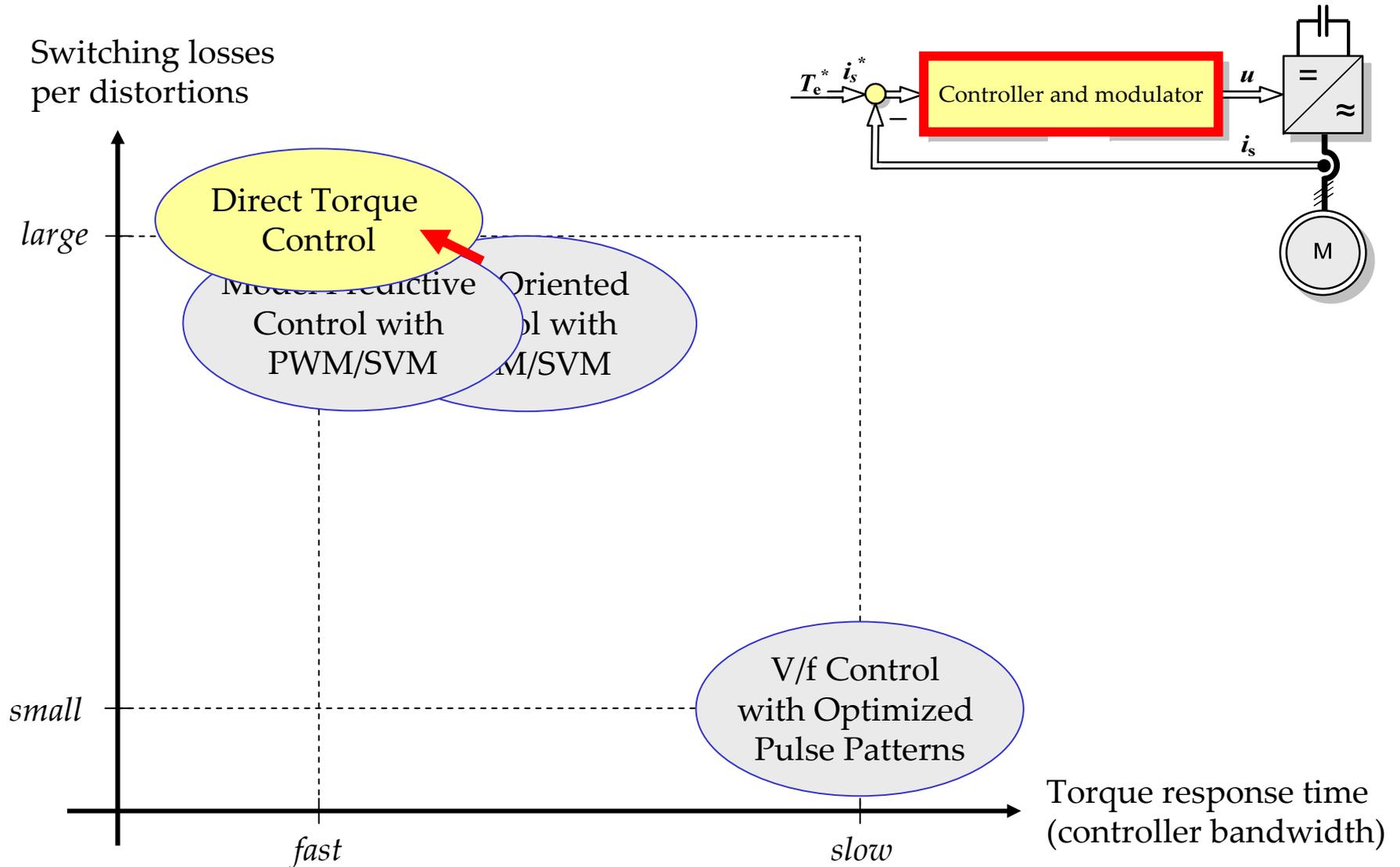
# Control and Modulation



# Control and Modulation

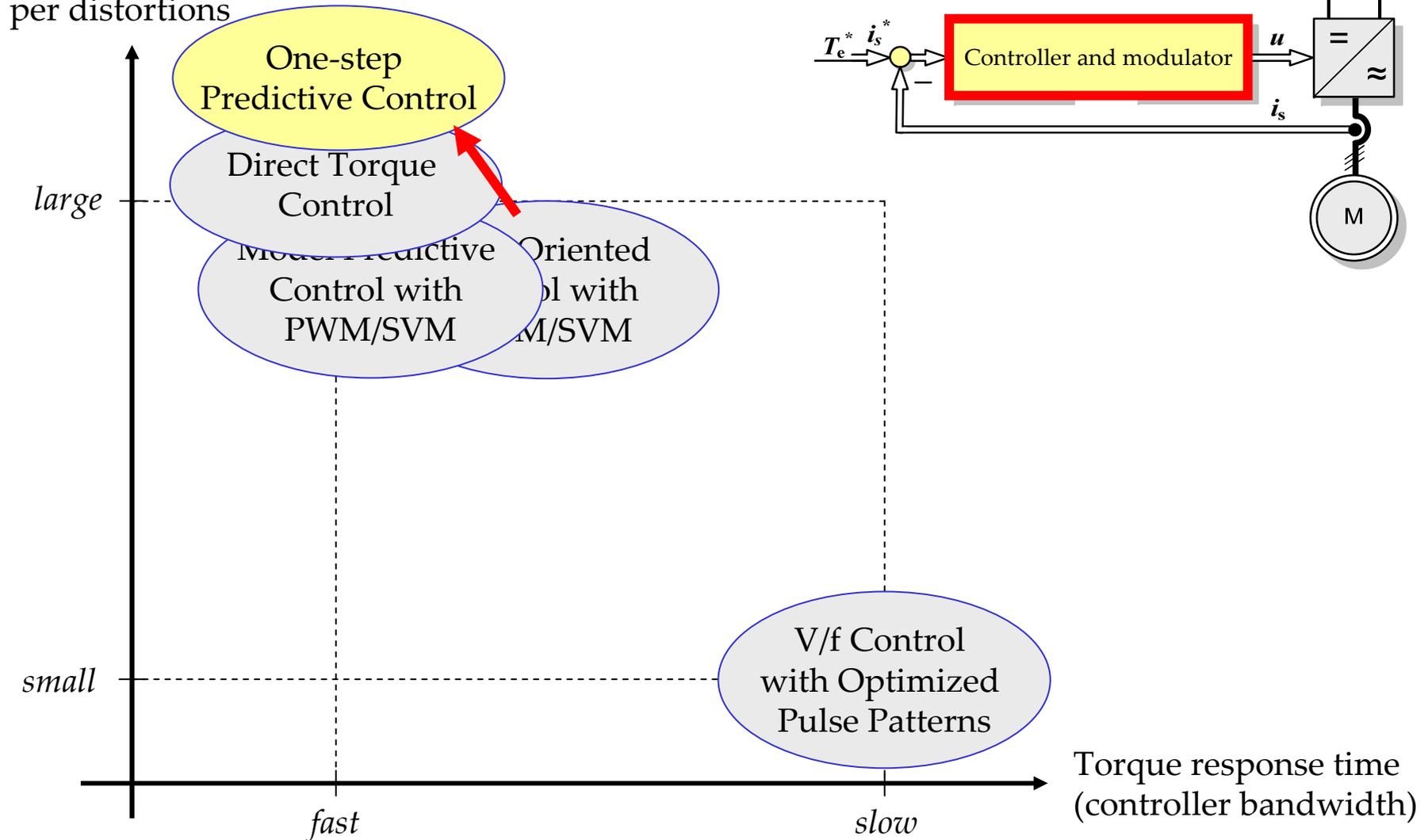


# Control and Modulation



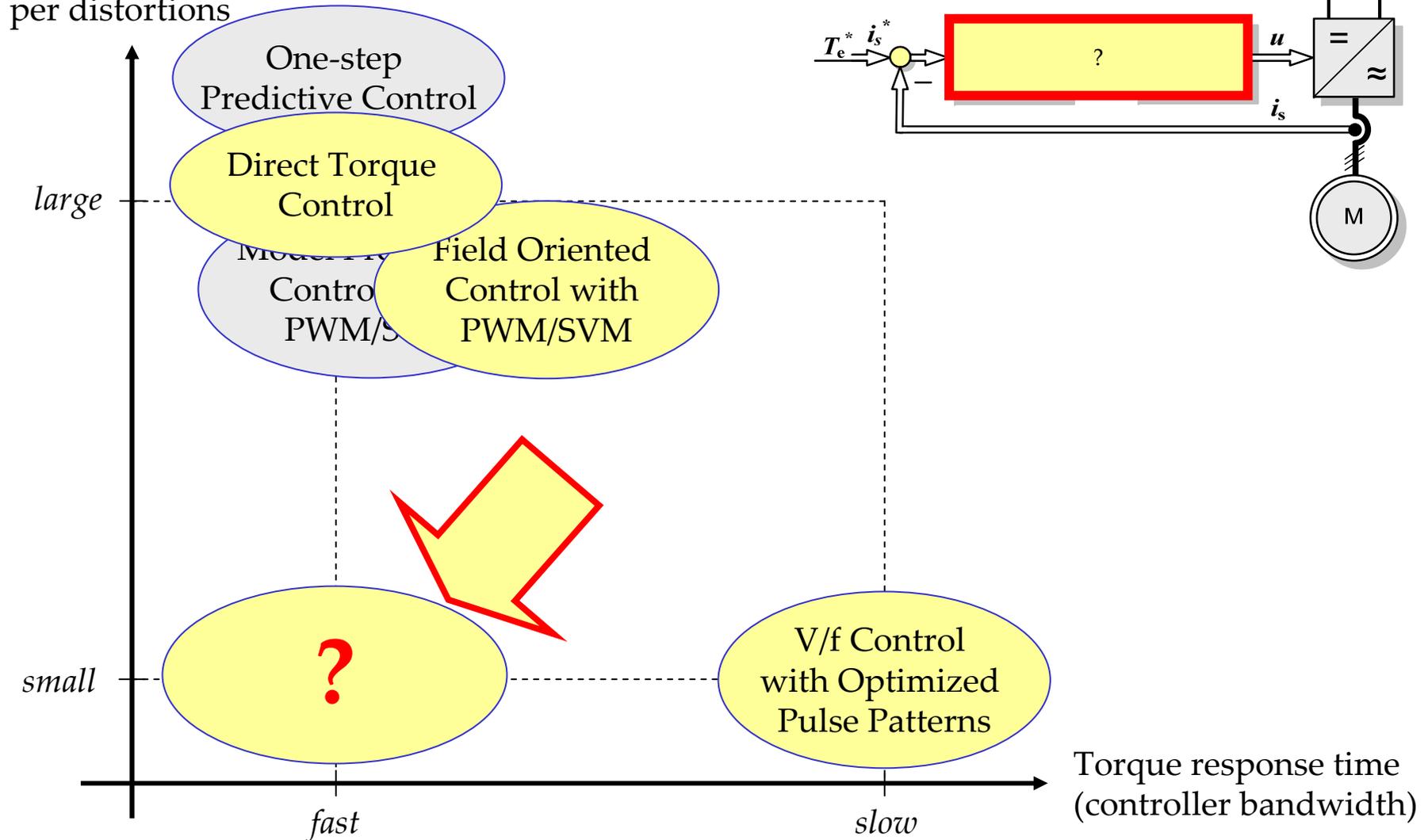
# Control and Modulation

Switching losses  
per distortions



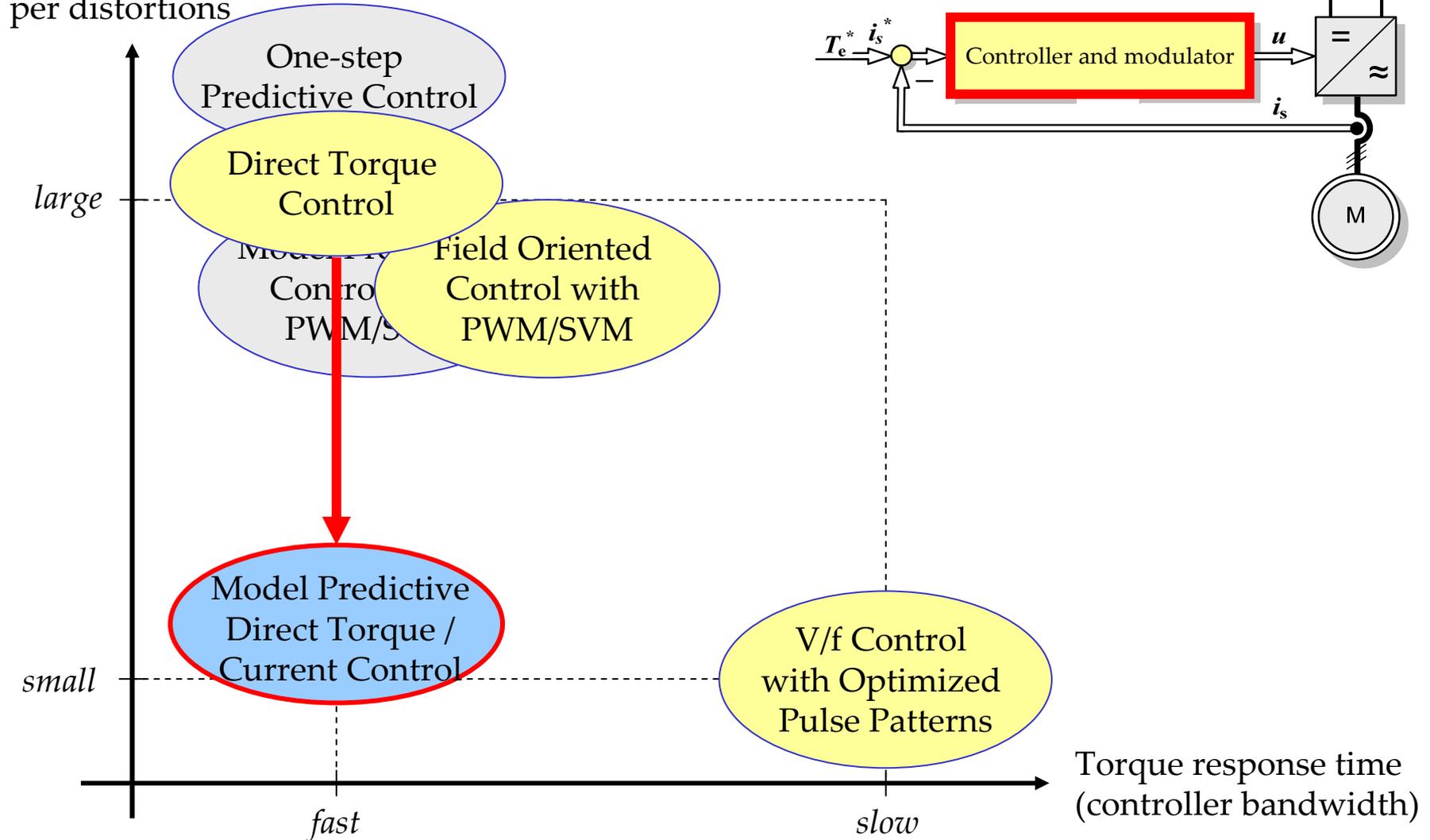
# Control and Modulation: Goal

Switching losses  
per distortions



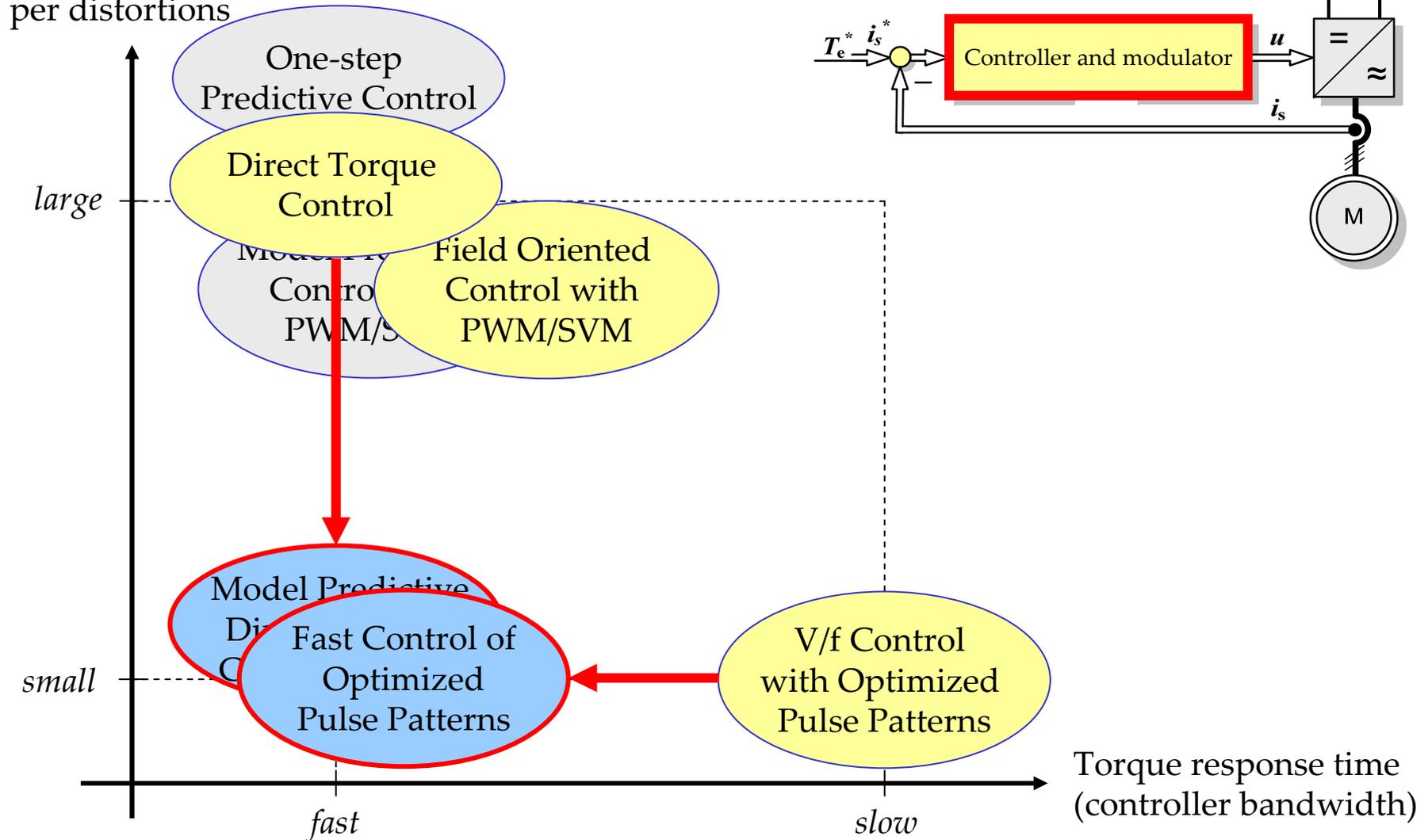
# Control and Modulation: New Methods

Switching losses  
per distortions



# Control and Modulation: New Methods

Switching losses  
per distortions



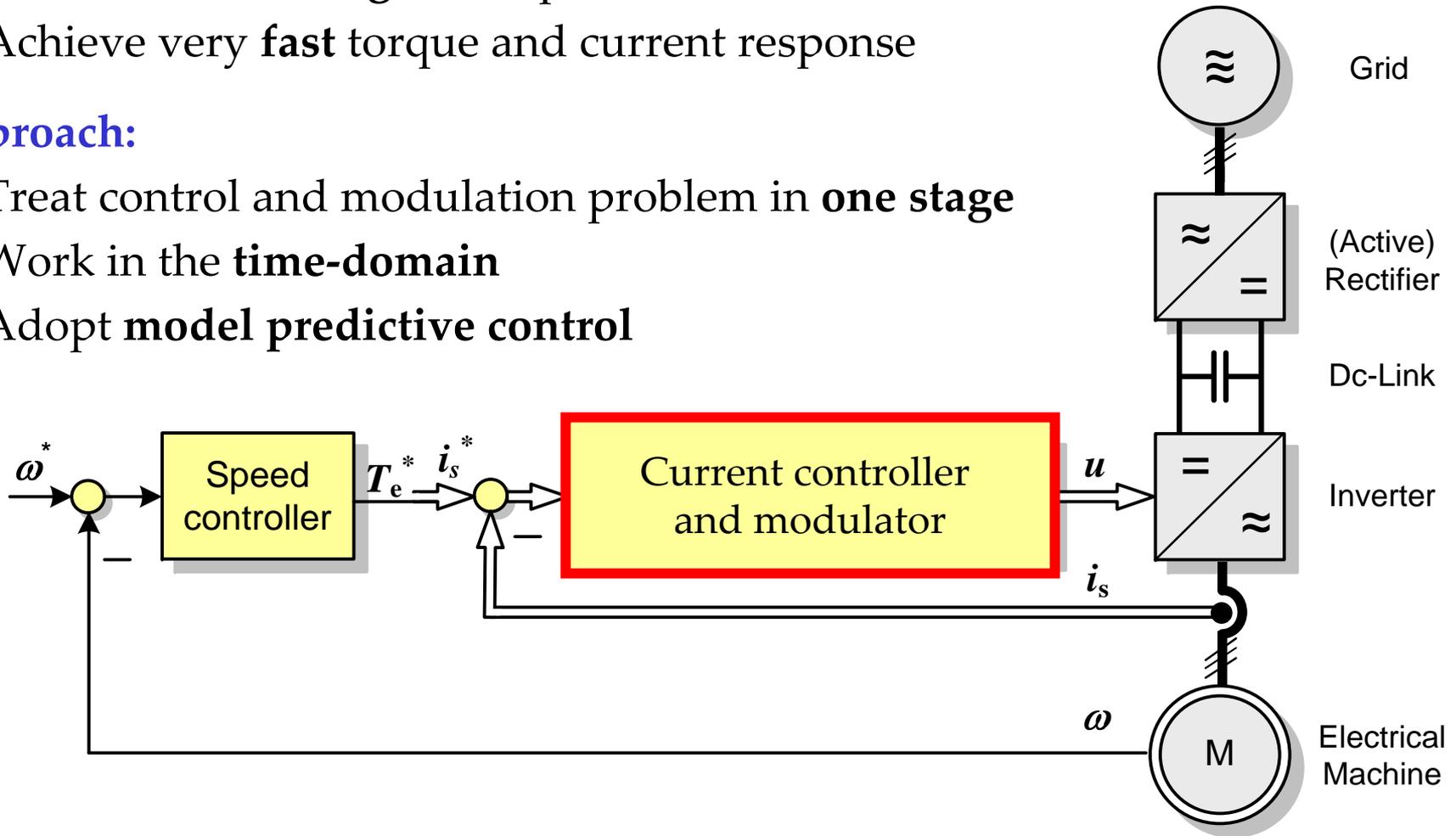
# Control and Modulation: New Methods

**Goal:** Fully utilize capability of drive hardware

- Minimize **switching losses** per **distortions**
- Achieve very **fast** torque and current response

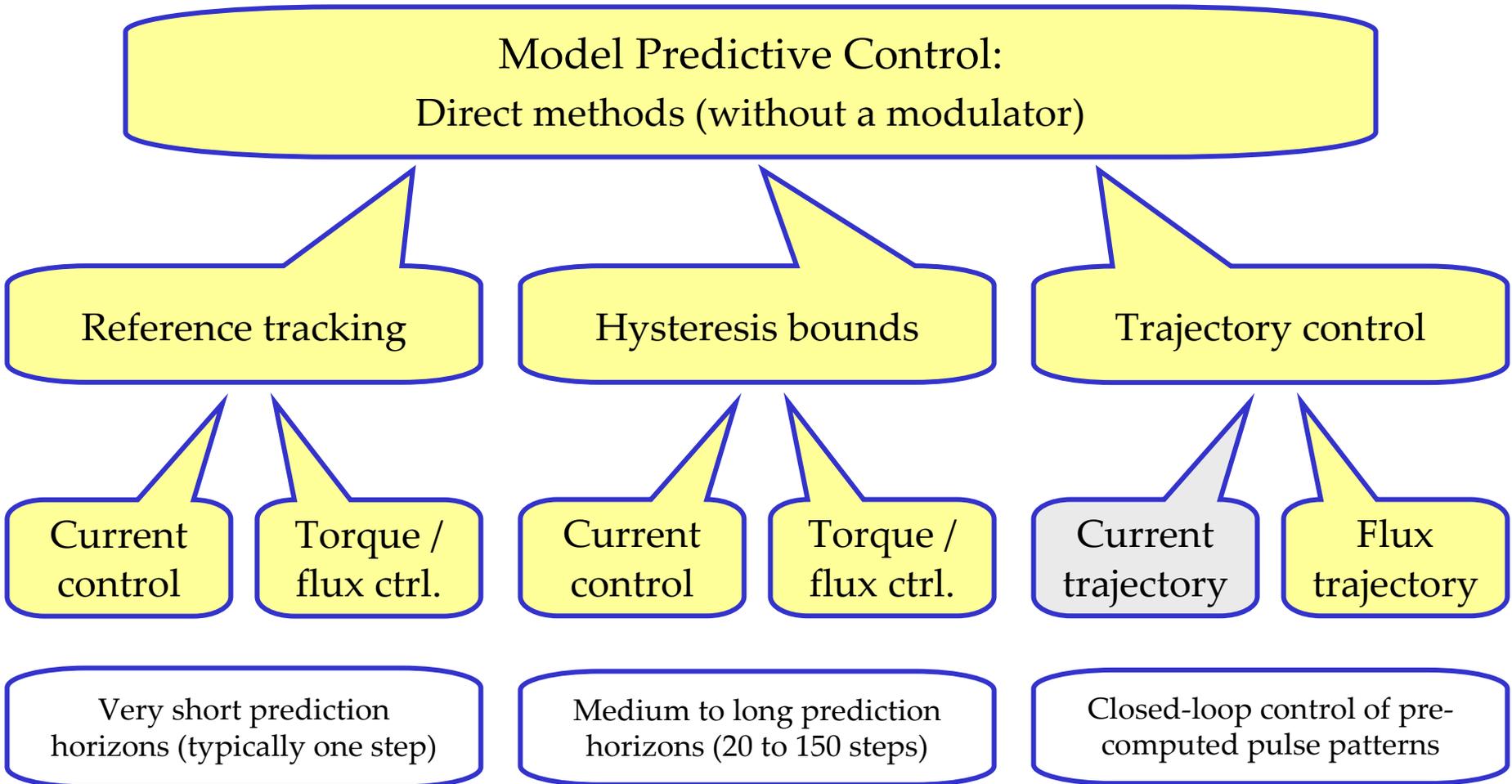
**Approach:**

- Treat control and modulation problem in **one stage**
- Work in the **time-domain**
- Adopt **model predictive control**



**Model Predictive Control**  
*for MV Electrical Drives*

# Classification of MPC Schemes for Electrical Drives



# Classification of MPC Schemes for Electrical Drives

Model Predictive Control:  
Direct methods (without a modulator)

Reference tracking

Hysteresis bounds

Trajectory control

Current control

Torque /  
flux ctrl.

Current control

Torque /  
flux ctrl.

Current trajectory

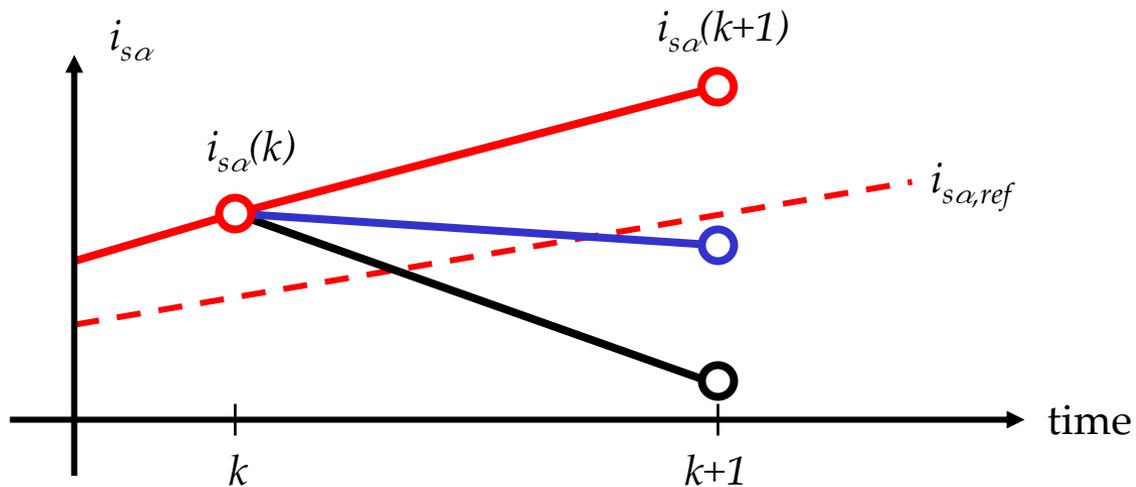
Flux trajectory

Very short prediction horizons (typically one step)

Medium to long prediction horizons (20 to 150 steps)

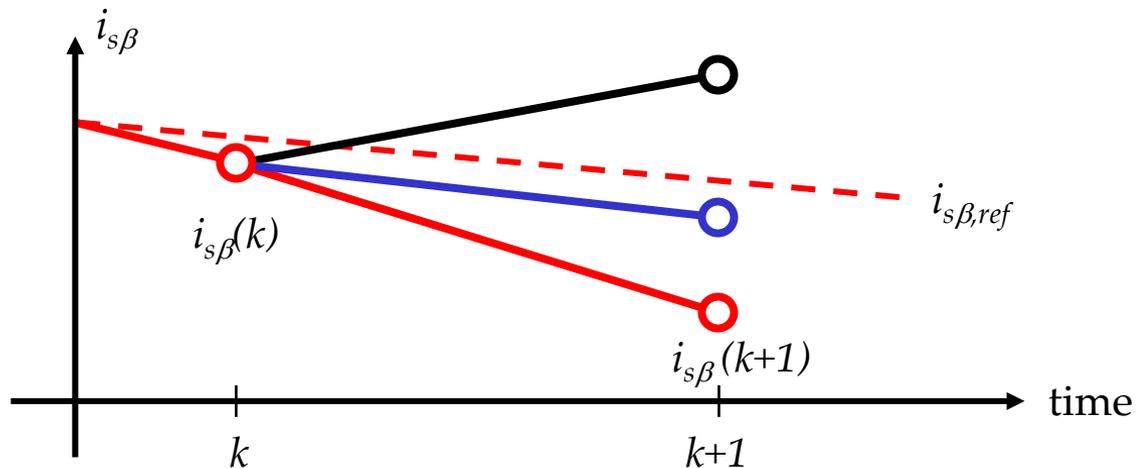
Closed-loop control of pre-computed pulse patterns

# One-Step Predictive Current Control



## Algorithm

- Enumerate all 27 switch transitions
- Predict currents at  $k+1$
- Choose switch transition with minimal current error at  $k+1$



# One-Step Predictive *Current* Control

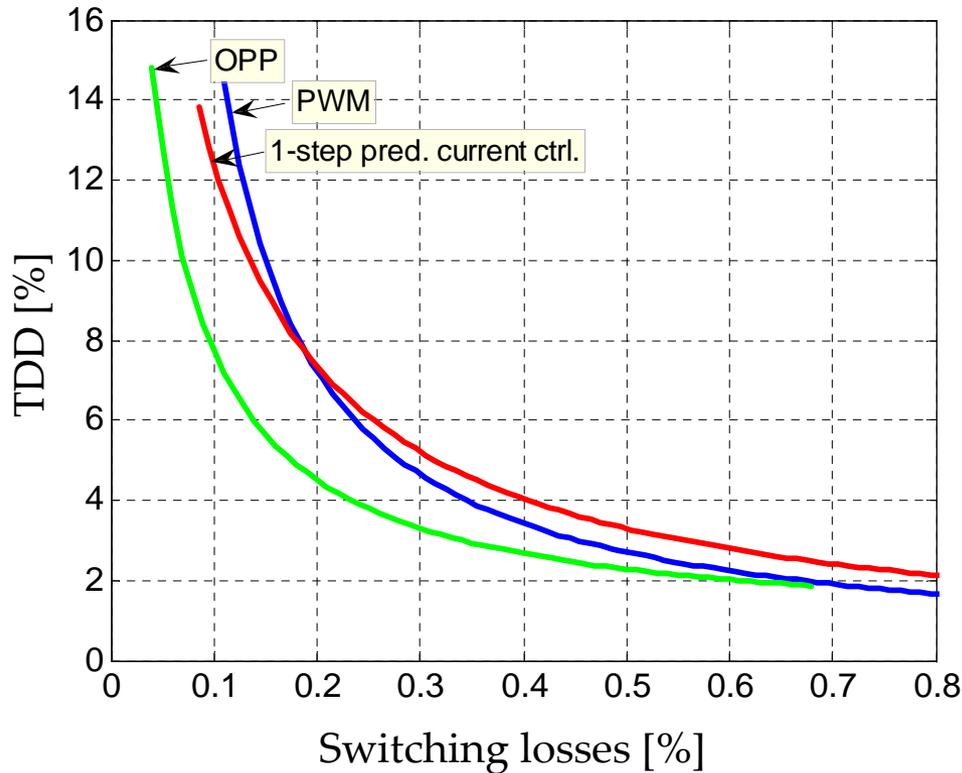
**Performance Index:**  $J^*(x(k)) := \min_{u_k} \underbrace{\|i_e(k+1)\|_1}_{\text{Deviation from current reference}} + \lambda_n \underbrace{\|\Delta u(k)\|_1}_{\text{Penalty on switching effort}}$

**Constraints**  $\left\{ \begin{array}{l} i_s(k+1) = A_1 i_s(k) + A_2 \psi_r(k) + B u(k), \text{ Model of machine} \\ u(k) \in \{-1, 0, 1\}^3, \text{ Discrete-valued switch positions} \\ u(k) \in \mathcal{U}(u(k-1)) \text{ Restrictions on switch transitions} \end{array} \right.$

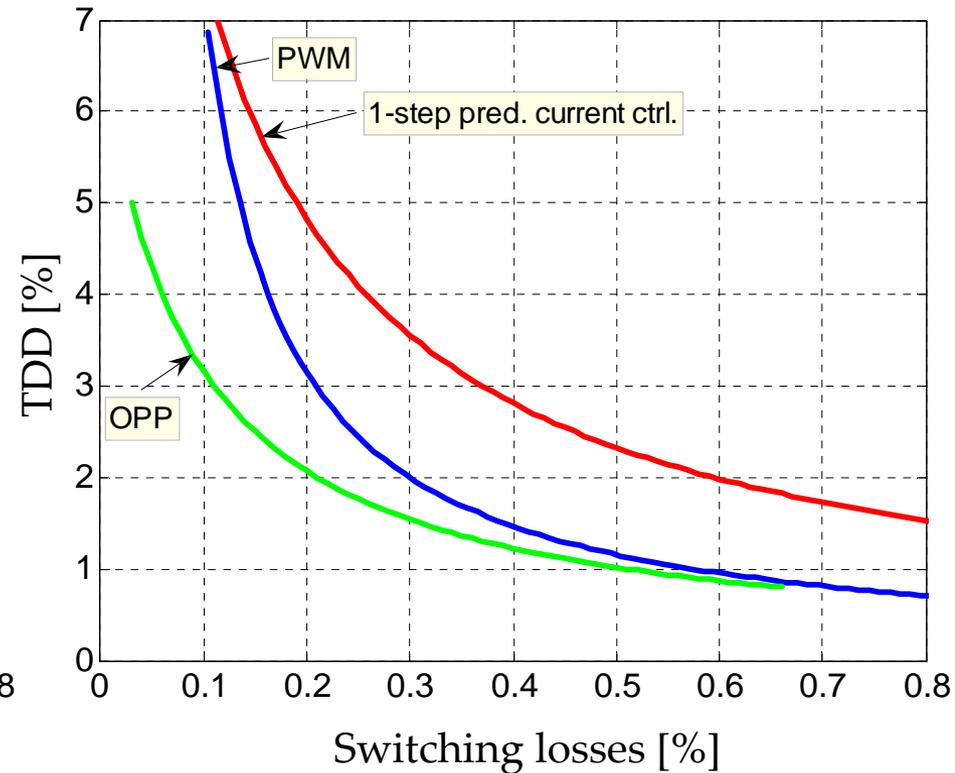
- Main features:**
- prediction **horizon** is one
  - machine **model**
  - **minimization** of switching effort (e.g. frequency)
  - $\lambda_n \Rightarrow$  trade-off between tracking accuracy and switching
  - conceptually and computationally **very simple**

# One-step Predictive Current Control

## Current TDD vs switching losses



## Torque TDD vs switching losses



- Current THD similar to PWM
- Torque THD significantly worse than PWM

# Classification of MPC Schemes for Electrical Drives

Model Predictive Control:  
Direct methods (without a modulator)

Reference tracking

Hysteresis bounds

Trajectory control

Current control

Torque / flux ctrl.

Current control

Torque / flux ctrl.

Current trajectory

Flux trajectory

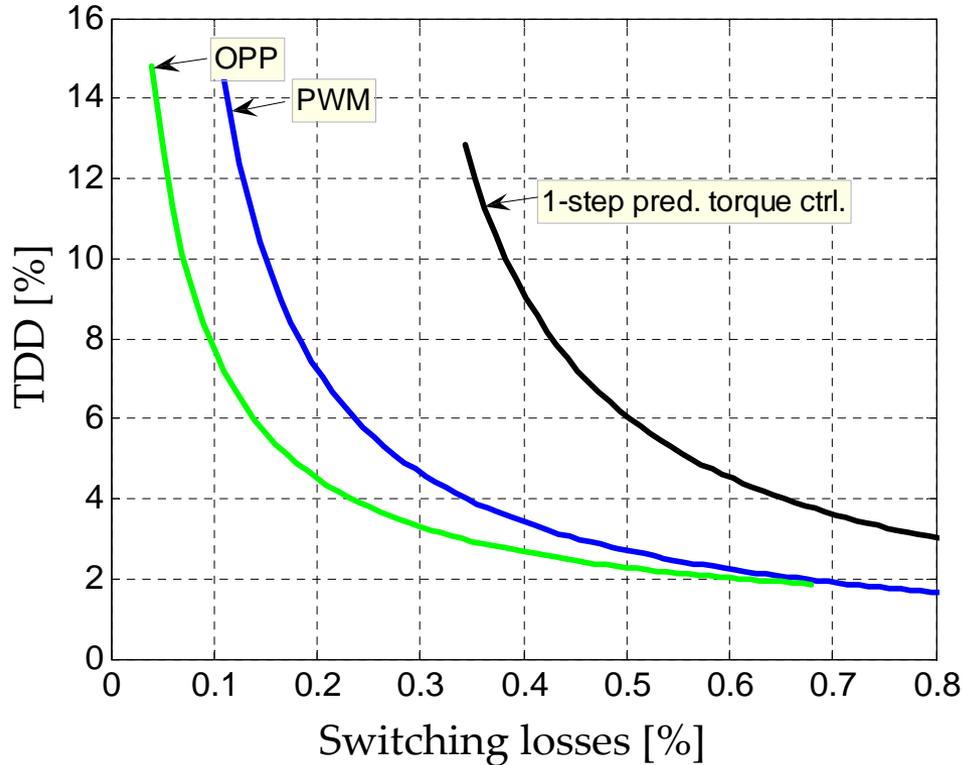
Very short prediction horizons (typically one step)

Medium to long prediction horizons (20 to 150 steps)

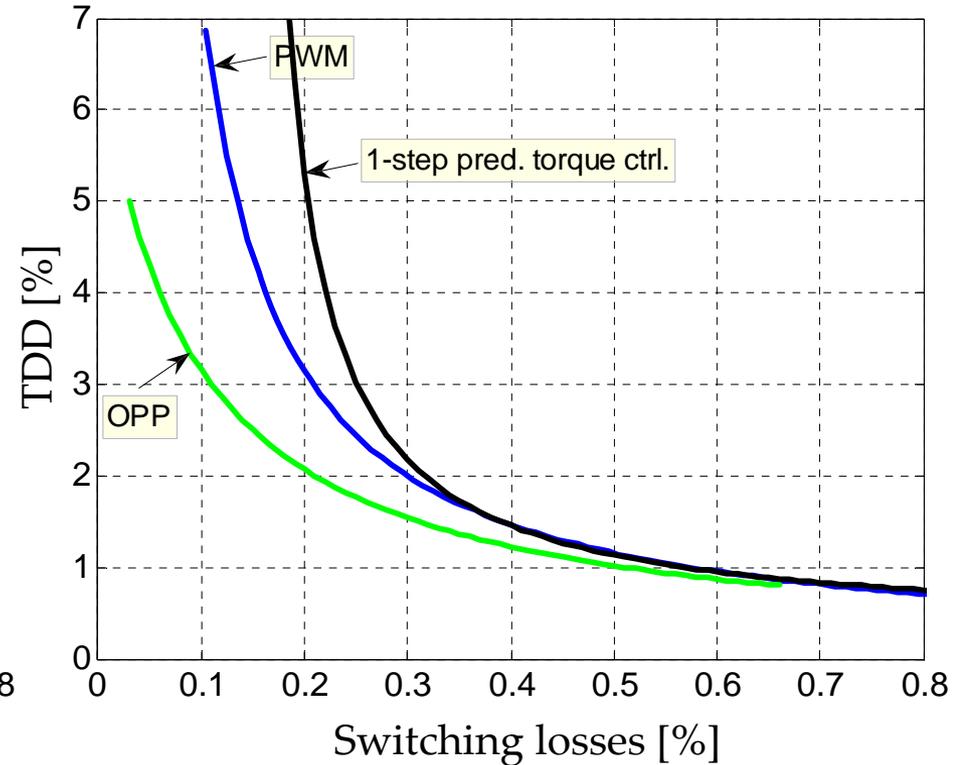
Closed-loop control of pre-computed pulse patterns

# One-step Predictive Torque Control

## Current TDD vs switching losses



## Torque TDD vs switching losses



- Torque THD similar to PWM
- Current THD significantly worse than PWM

# Classification of MPC Schemes for Electrical Drives

Model Predictive Control:  
Direct methods (without a modulator)

Reference tracking

Hysteresis bounds

Trajectory control

Current control

Torque / flux ctrl.

Current control

Torque / flux ctrl.

Current trajectory

Flux trajectory

Very short prediction horizons (typically one step)

Medium to long prediction horizons (20 to 150 steps)

Closed-loop control of pre-computed pulse patterns

# Model Predictive Direct Current Control: Step 1

Predict current trajectories for (all) possible switching sequences

## Key ingredients:

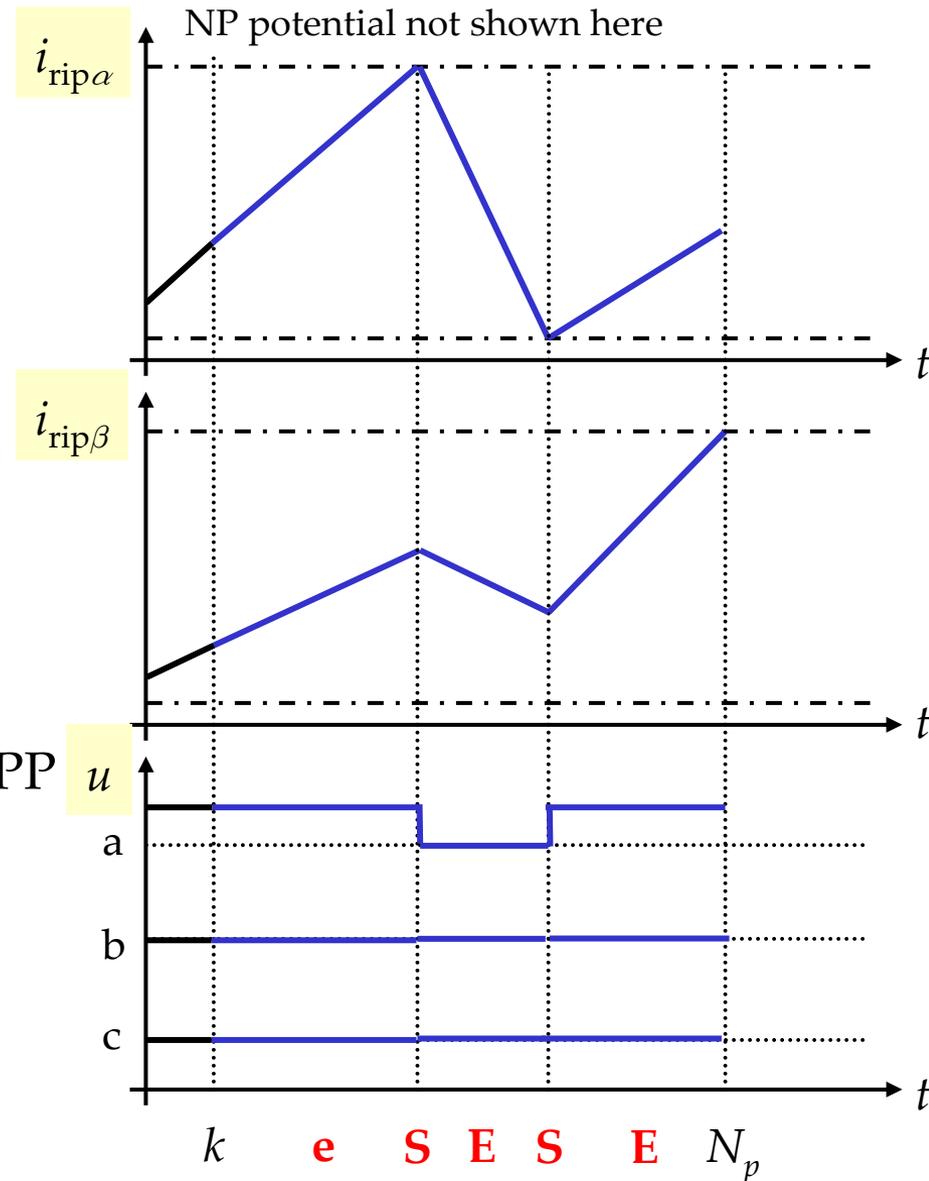
- Drive model
- Extrapolation

Switching horizon, e.g. 'eSESE'

- **S**: consider all switch transitions
- **E**: extrapolate/extend currents and NPP
- **e**: optional 'E'

Prediction horizon  $N_p$

Typically 50..150 time-steps



# Model Predictive Direct Current Control: Step 1

Predict current trajectories for (all) possible switching sequences

## Key ingredients:

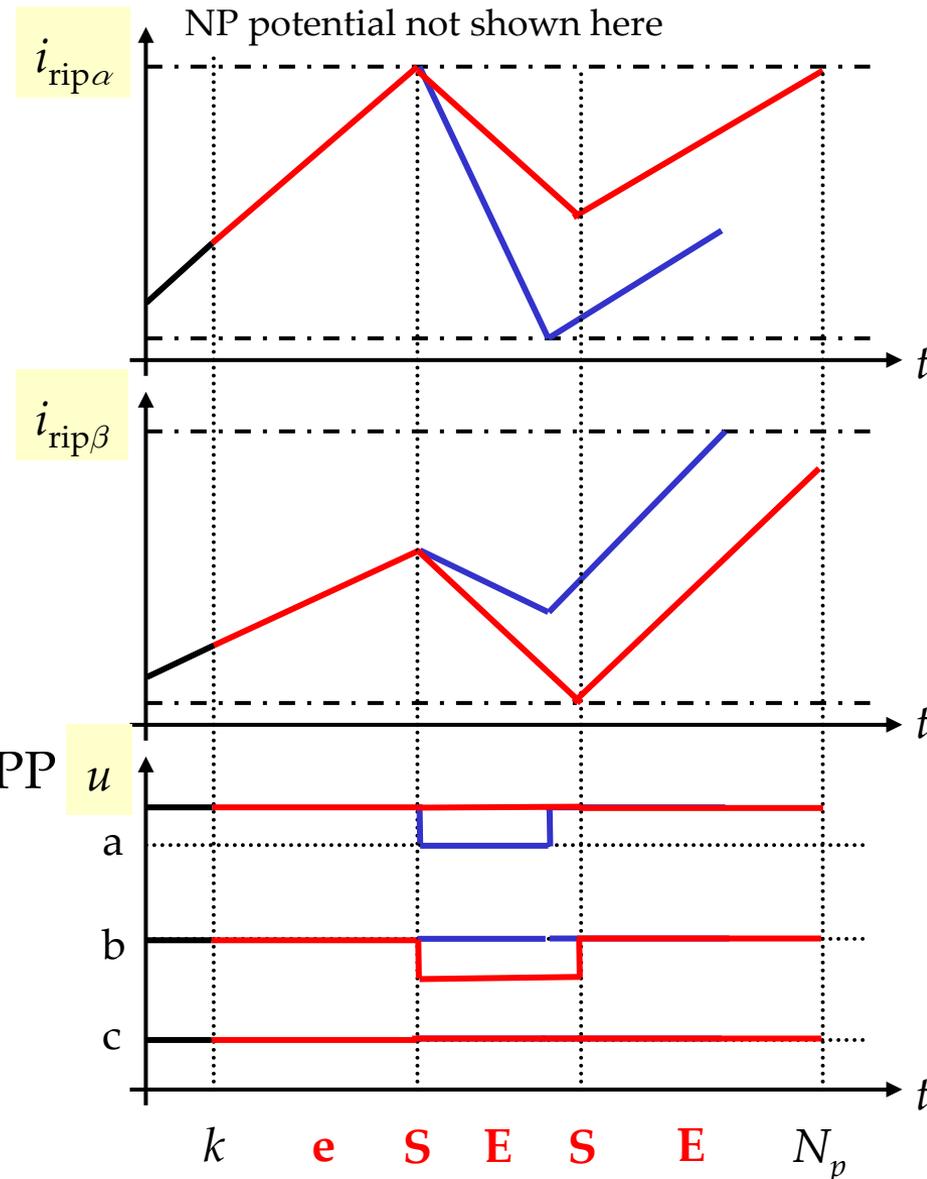
- Drive model
- Extrapolation

Switching horizon, e.g. 'eSESE'

- **S**: consider all switch transitions
- **E**: extrapolate/extend currents and NPP
- **e**: optional 'E'

Prediction horizon  $N_p$

Typically 50..150 time-steps

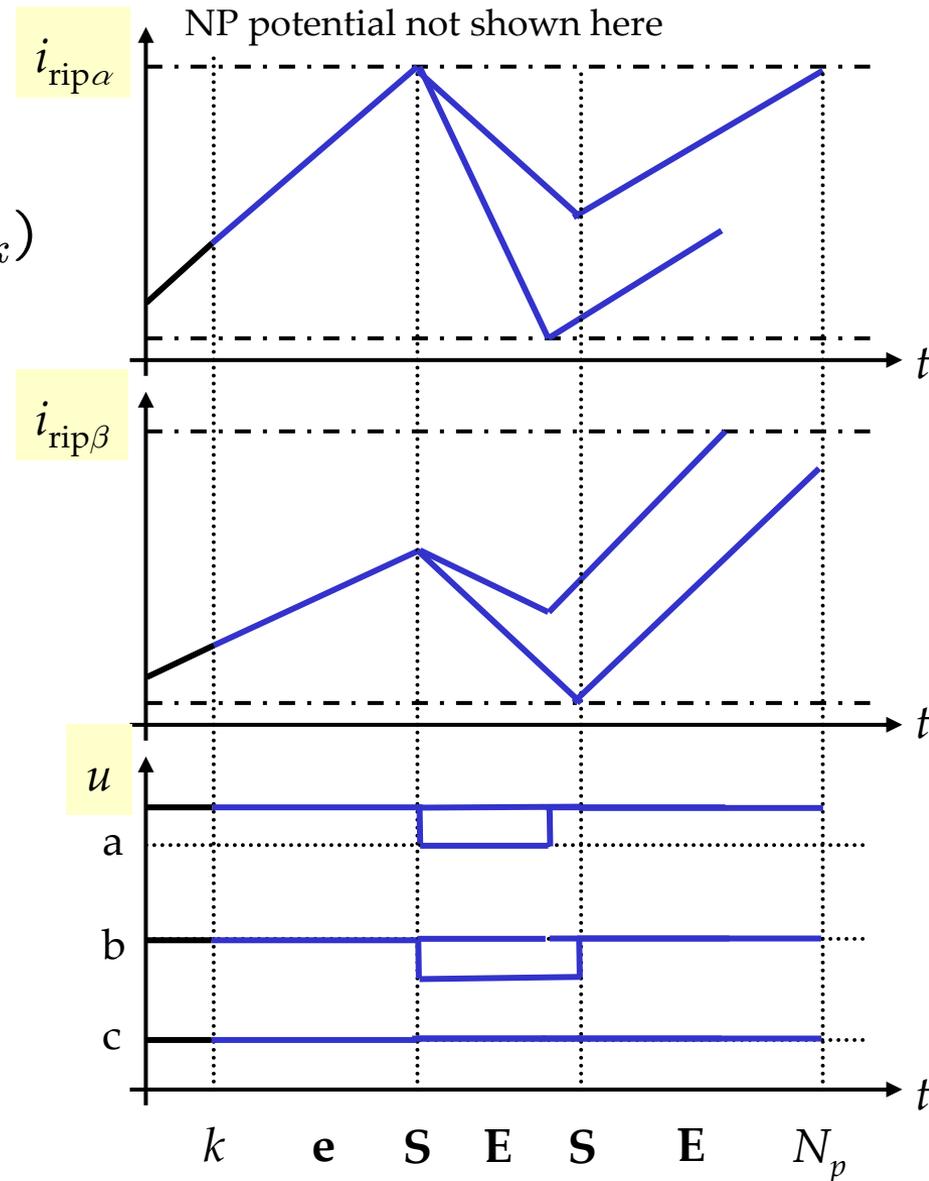


# Model Predictive Direct Current Control: Step 2

Evaluate and **minimize sw. losses**

$$J^*(x) := \min_U \frac{1}{N_p} \sum_{k=0}^{N_p-1} E_{\text{loss}}(x_k, u_k)$$

=> Optimal **switching sequence**  $U$



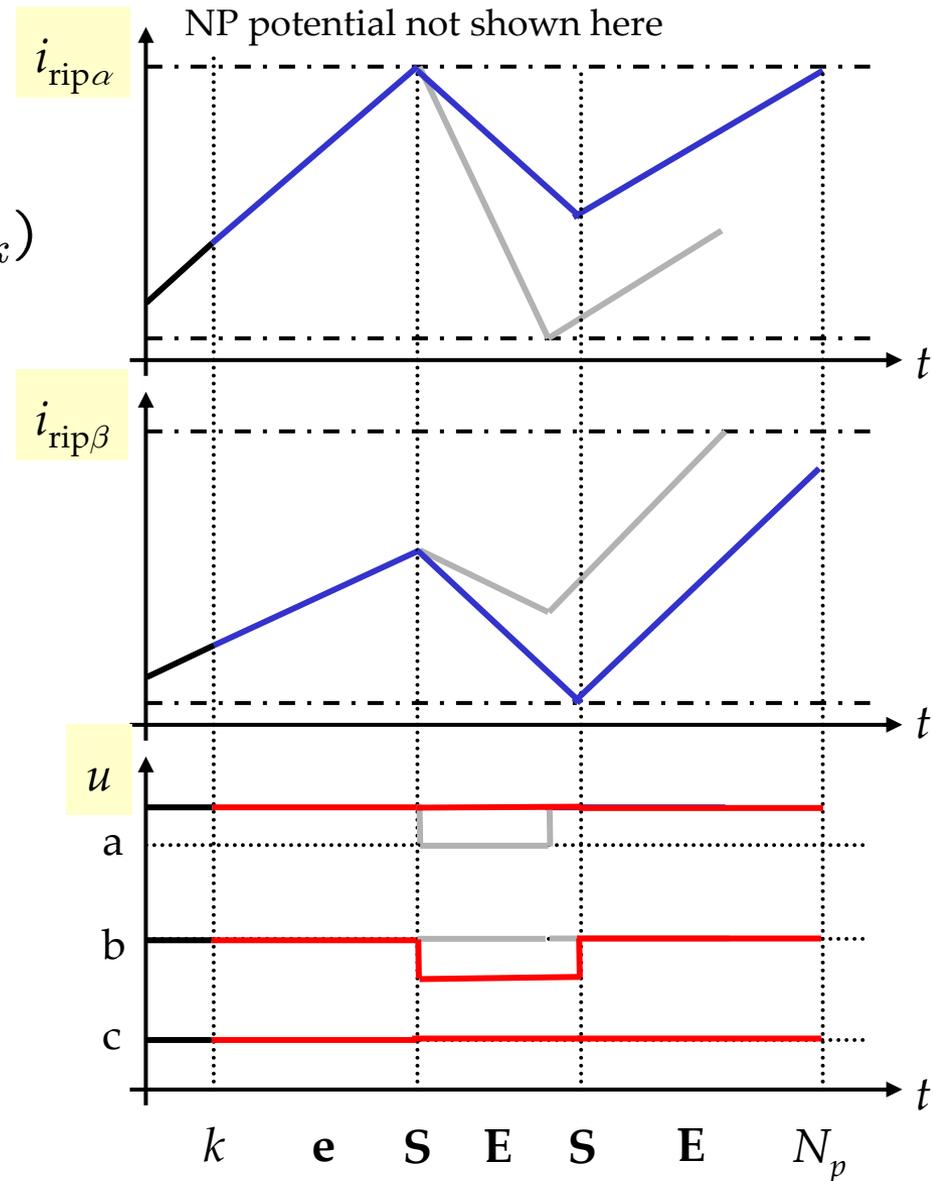
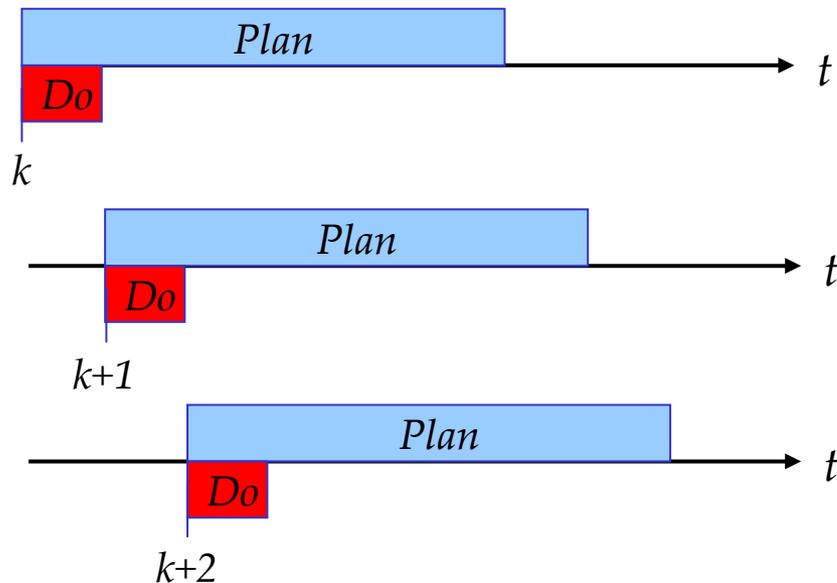
# Model Predictive Direct Current Control: Steps 2 & 3

Evaluate and **minimize sw. losses**

$$J^*(x) := \min_U \frac{1}{N_p} \sum_{k=0}^{N_p-1} E_{\text{loss}}(x_k, u_k)$$

=> Optimal **switching sequence**  $U$

Apply only the **first element** of  $U$



# Model Predictive Direct Current Control

**Performance Index:**  $J^*(x) := \min_U \underbrace{\frac{1}{N_p} \sum_{k=0}^{N_p-1} E_{\text{loss}}(x_k, u_k)}_{\text{Short-term avg. switching losses (power)}}$

Short-term avg. switching losses (power)

## Constraints

$\forall k = 0, \dots, N - 1$

$$\left\{ \begin{array}{ll} x_{k+1} = f(x_k, u_k), & \text{Model of machine and inverter} \\ y_k = g(x_k), & \text{Outputs (currents and NP)} \\ y_k \in \mathcal{Y}, & \text{Bounds on currents and NP} \\ u_k \in \{-1, 0, 1\}^3, & \text{Discrete-valued switch positions} \\ u_k \in \mathcal{U}(u_{k-1}) & \text{Restrictions on switch transitions} \end{array} \right.$$

- Main features:**
- short **switching** horizon but long **prediction** horizon
  - **models** of machine, inverter and losses
  - **minimization** of switching losses
  - **receding horizon** policy
  - **tailored** online solution approach

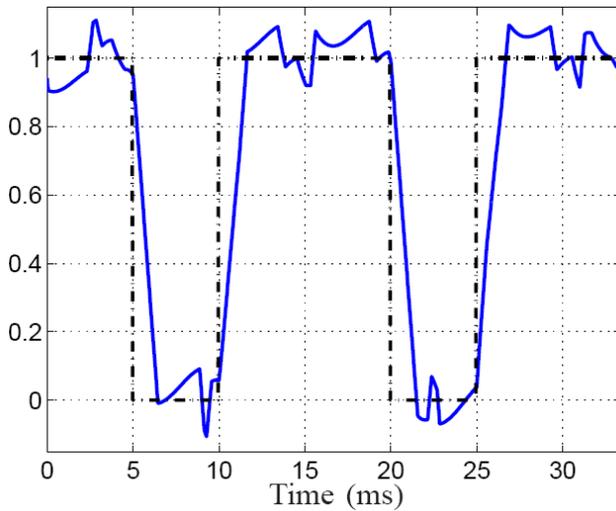
# Performance during Transients

3-level NPC inverter with 2MVA induction machine

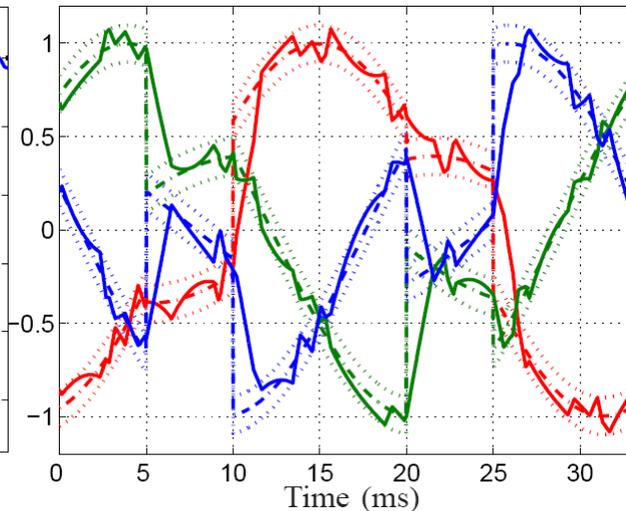
**Speed:**  $w_e=0.6$  pu

**Torque:** reference steps between  $T=1$  and  $0$  pu

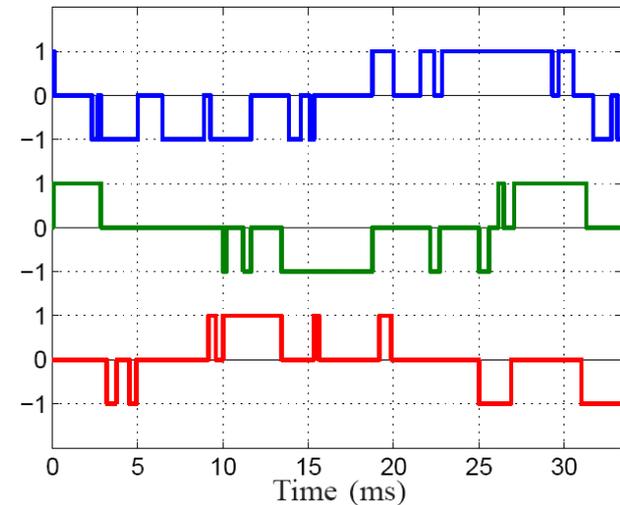
## Torque



## Stator currents



## Switch positions



Torque (current) response time of **2 ms**

# Performance at Steady-State

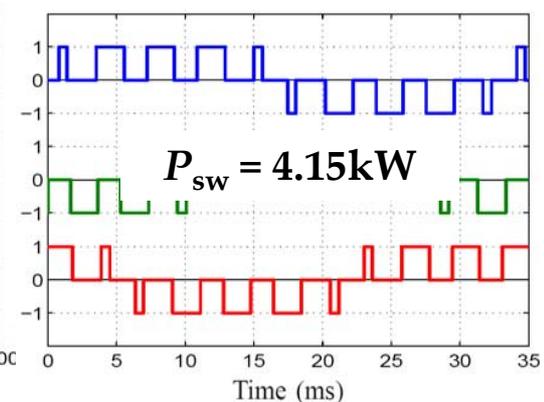
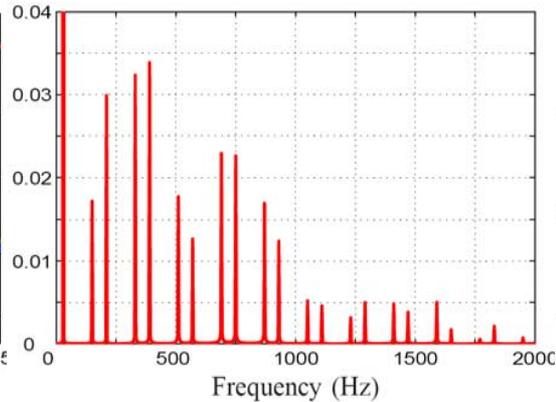
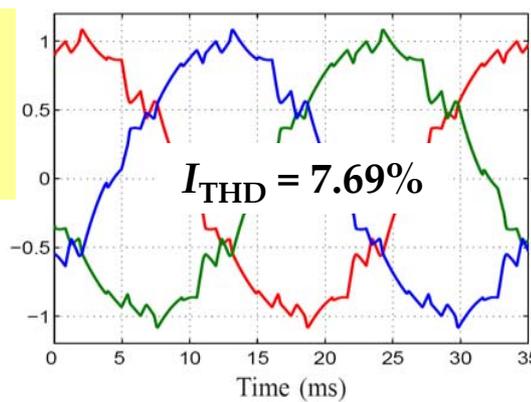
3-level NPC inverter with 2MVA ind. machine  
 $w_e=0.6$  pu,  $T_e=1$  pu

## Current

## Current spectrum

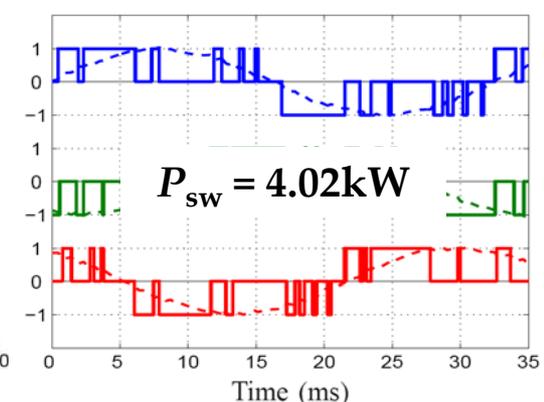
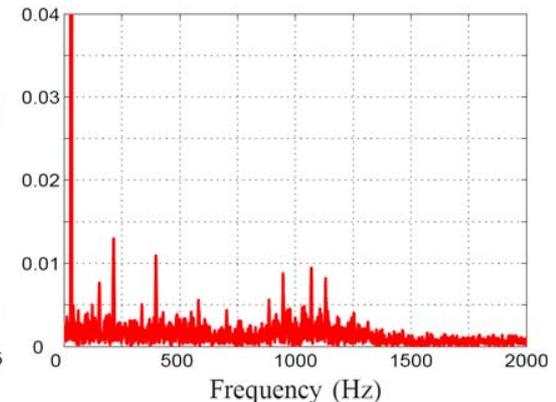
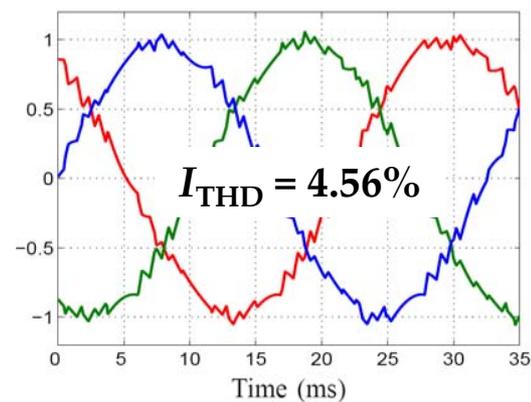
## Switch positions

FOC with  
PWM and  
 $f_c=270$  Hz



MPDCC  
'e(SE)<sup>3</sup>'

$N_p = 70$

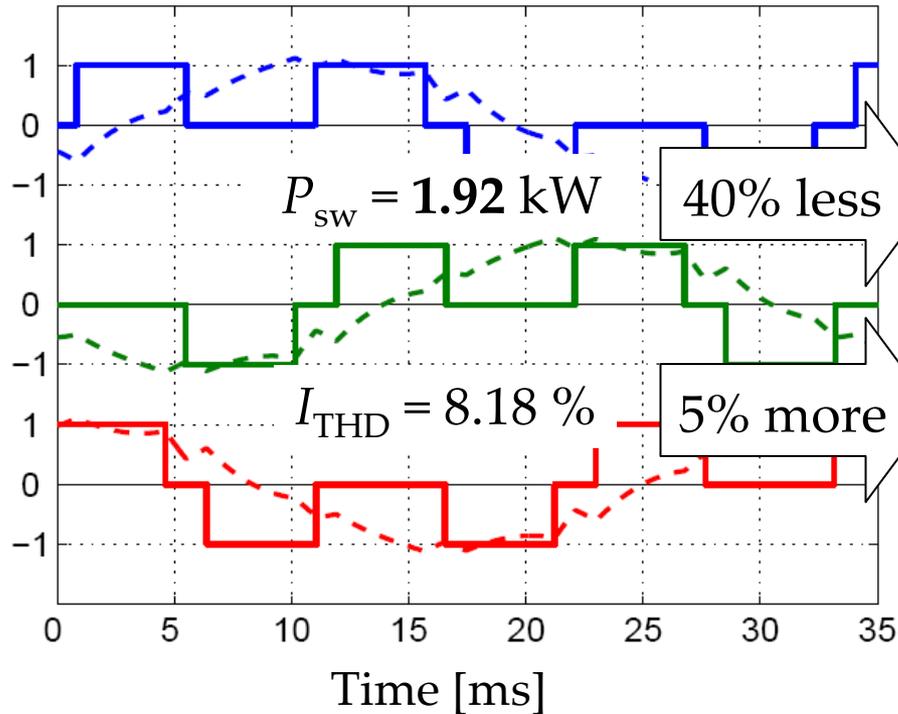


**Current THD reduced by 40% (for the same switching losses)**  
**Similar to optimal pulse patterns**

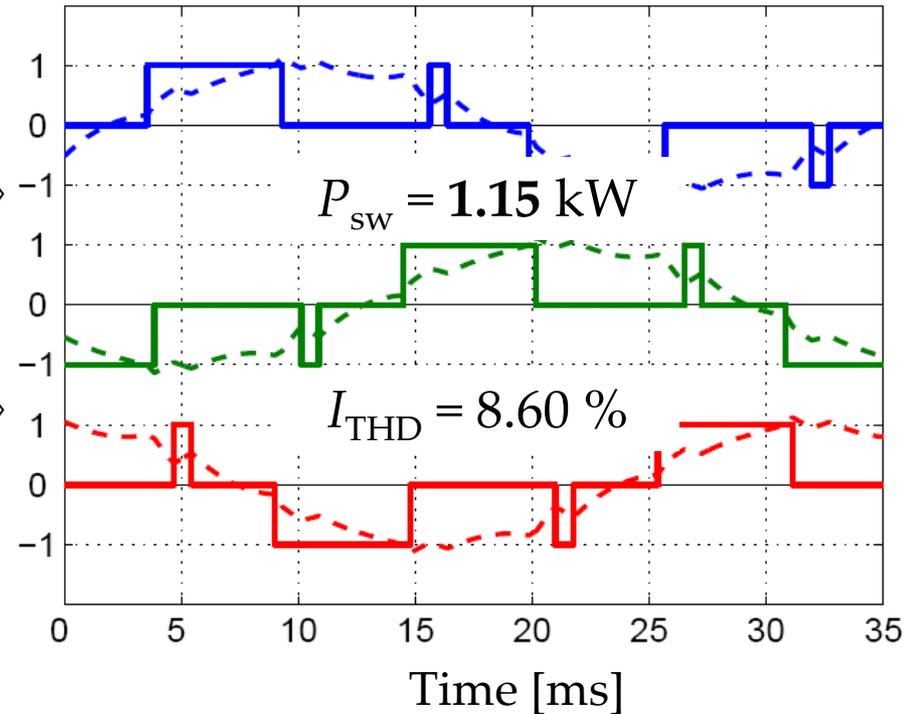
# MPDCC outperforming OPP

3-level NPC inverter with 2MVA ind. machine  
 $w_e=0.6$  pu,  $T_e=1$  pu

## Optimized Pulse Pattern



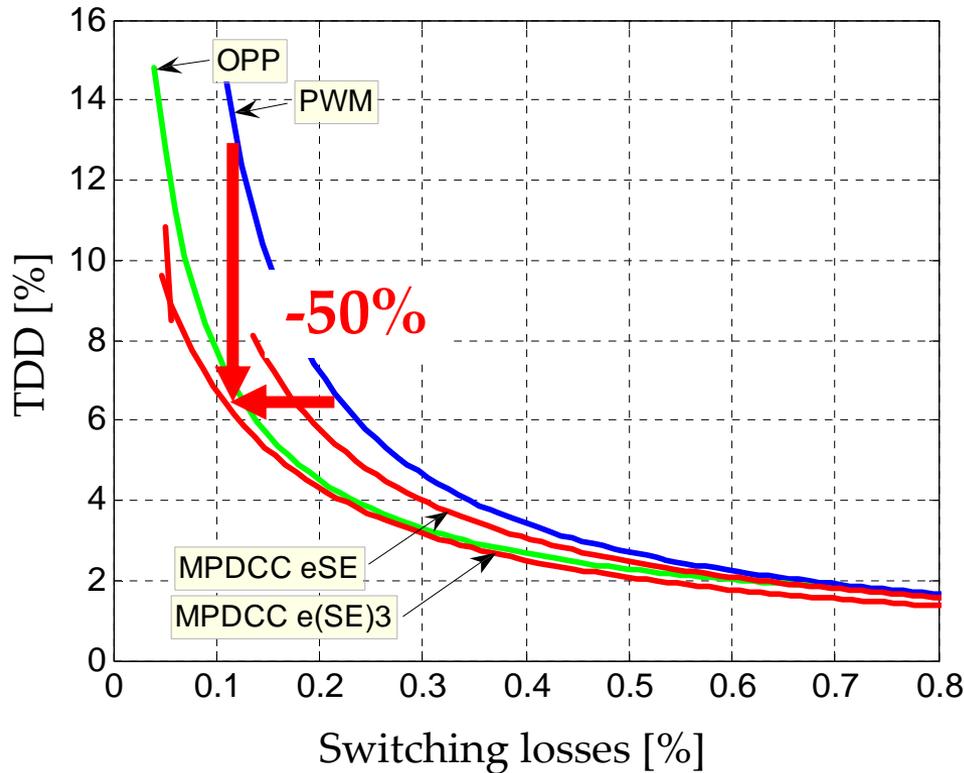
## Model Pred. Direct Current Ctrl.



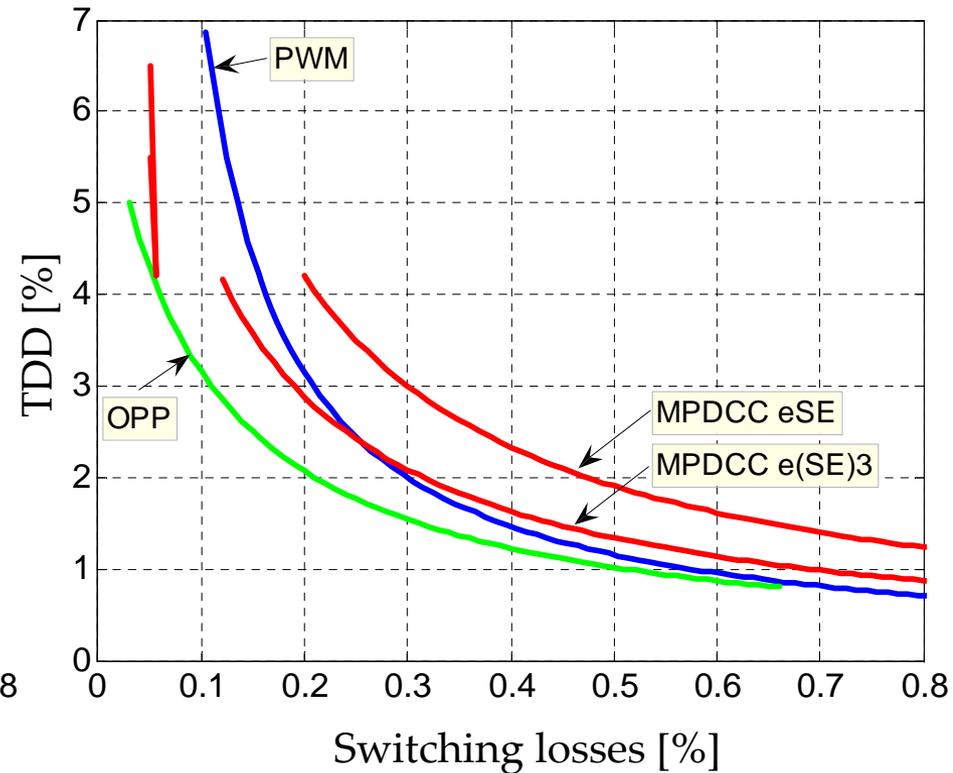
- OPPs: for a given switching *frequency*, minimize the current THD
- MPDCC: for a given current THD, minimize the switching *losses*

# Model Predictive Direct Current Control

## Current TDD vs switching losses

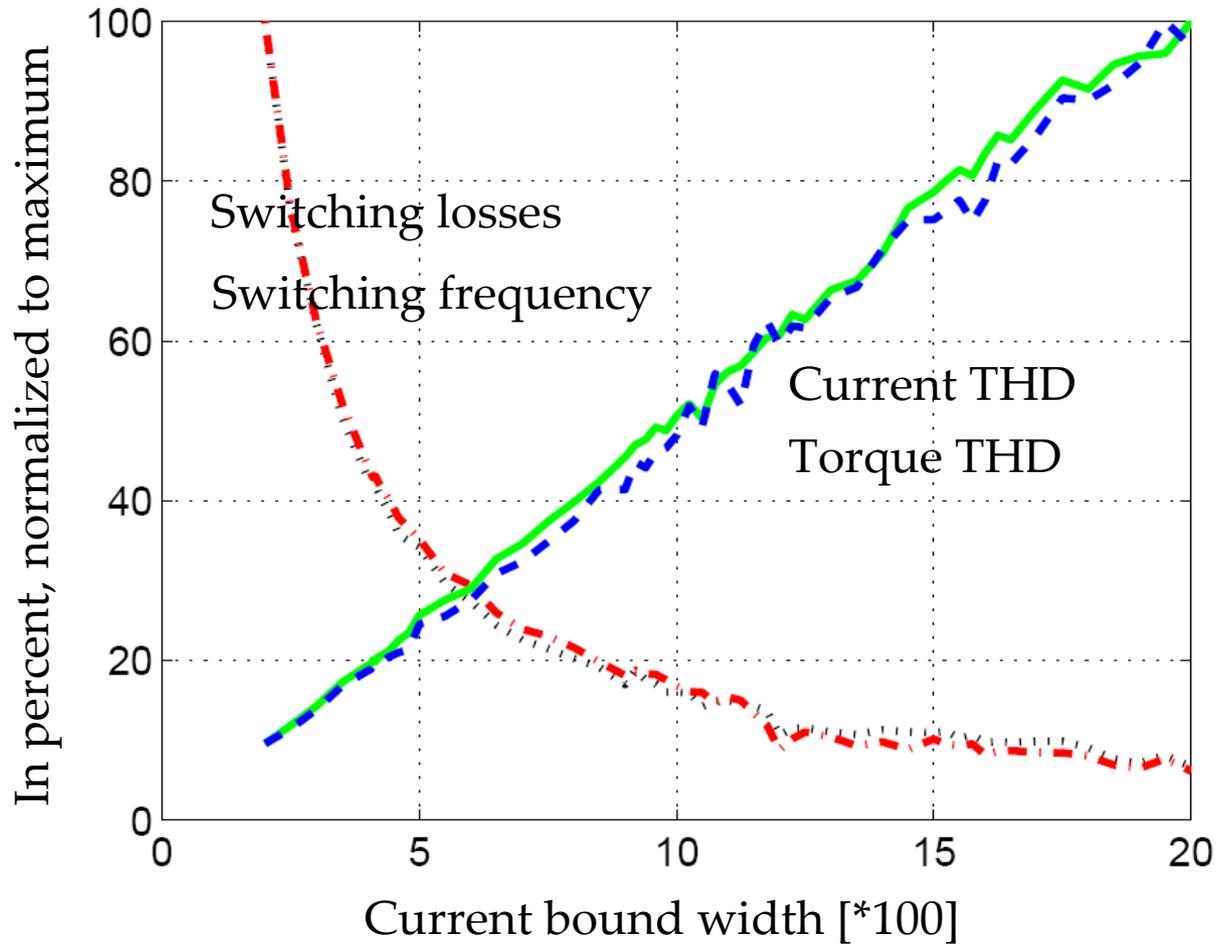


## Torque TDD vs switching losses



Long switching horizon eSESESE (50-150 steps):

- Current THD: better than with optimized pulse patterns
- Torque THD: similar to PWM



- Current and torque **distortions: linear** function of bound width
- **Switching frequency** (and losses): **hyperbolic** function of bound width

# Classification of MPC Schemes for Electrical Drives

Model Predictive Control:  
Direct methods (without a modulator)

Reference tracking

Hysteresis bounds

Trajectory control

Current control

Torque / flux ctrl.

Current control

Torque / flux ctrl.

Current trajectory

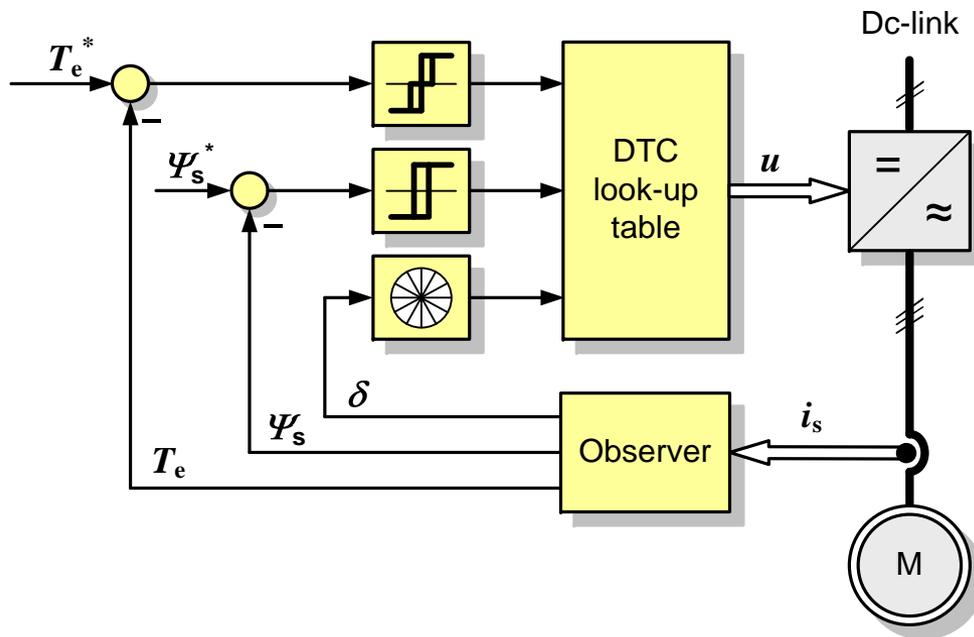
Flux trajectory

Very short prediction horizons (typically one step)

Medium to long prediction horizons (20 to 150 steps)

Closed-loop control of pre-computed pulse patterns

# Direct Torque Control

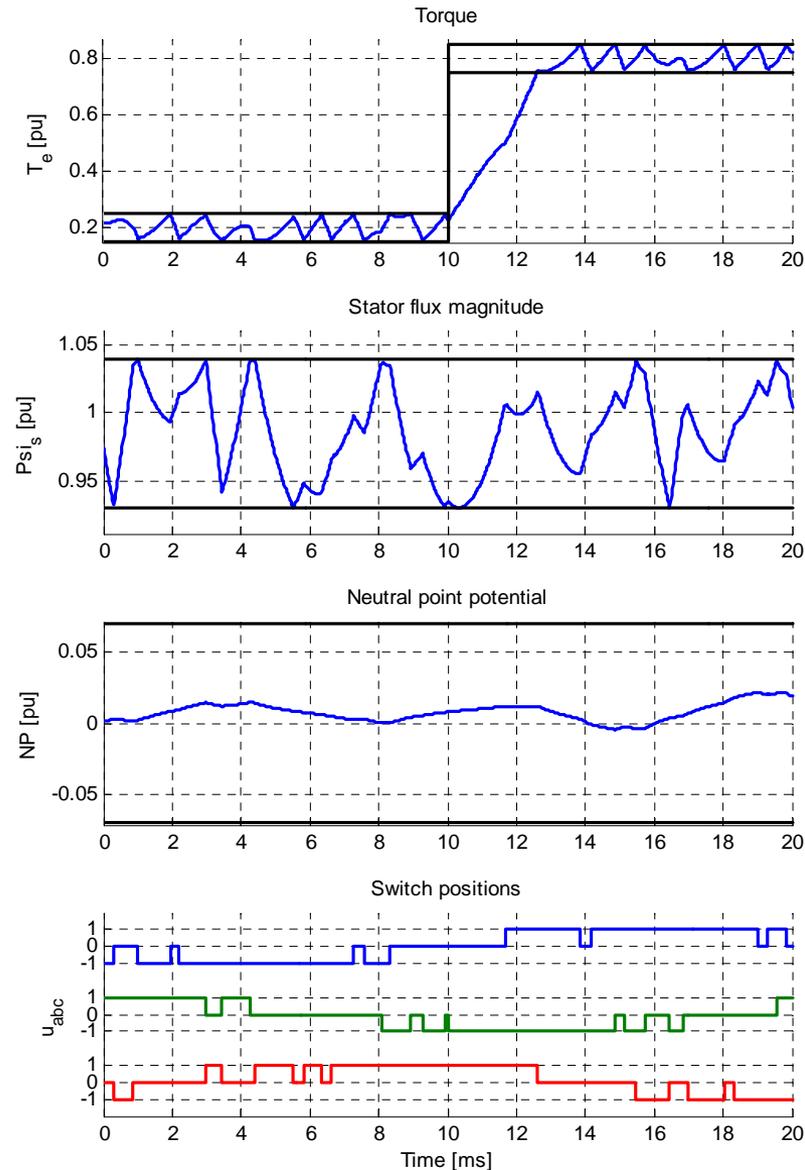


## Control objectives:

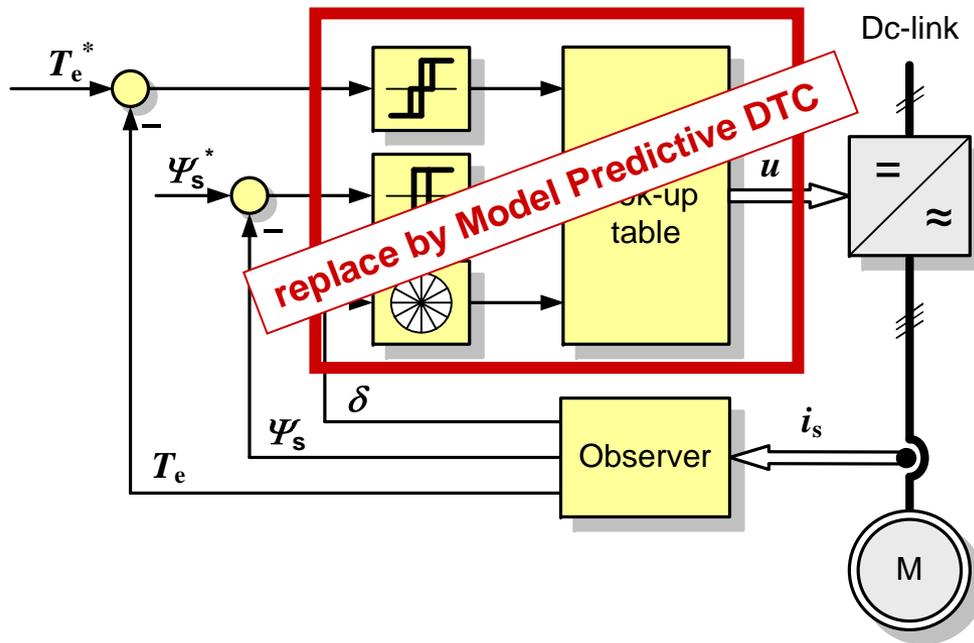
- Keep **torque**, **stator flux** and **neutral point potential** within given bounds
- Minimize the **switching losses**

## Control variable:

- Discrete inverter **switch positions**

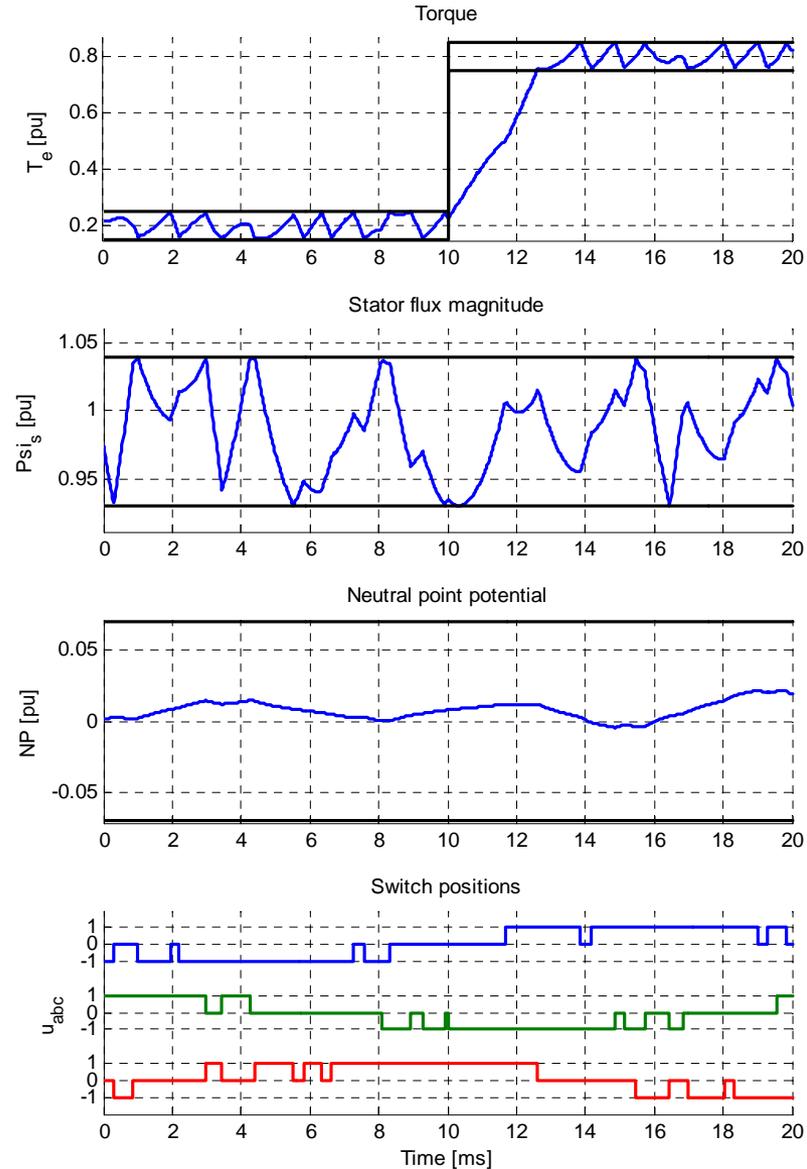


# Model Predictive Direct Torque Control



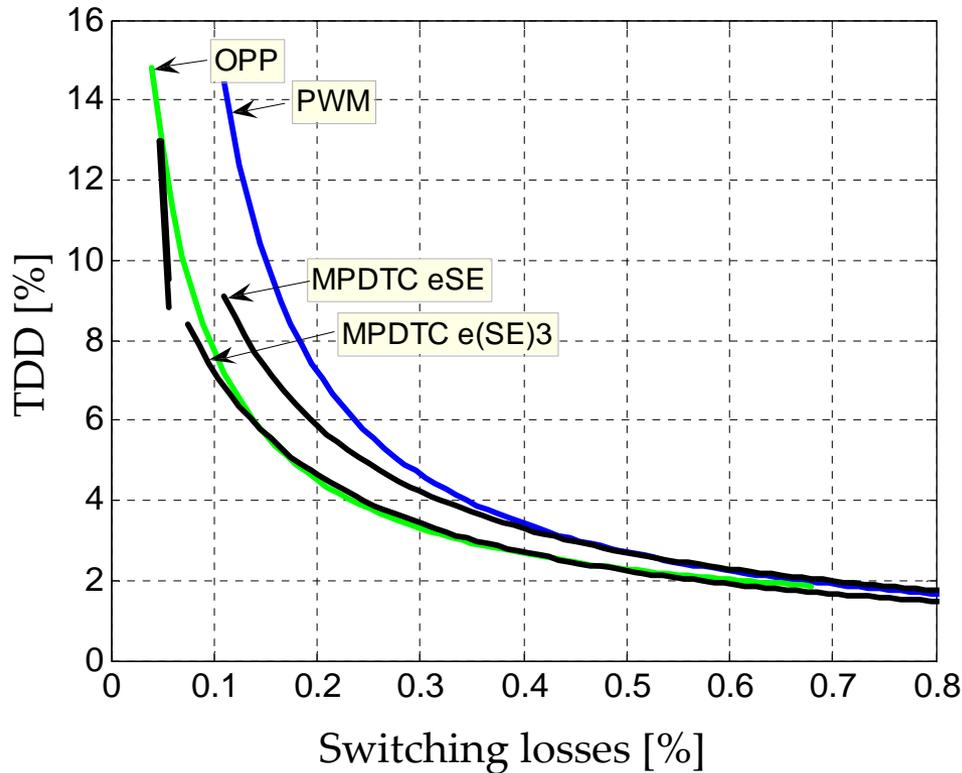
## Challenging control problem:

- Nonlinear
- Hybrid
- MIMO
- Sampling interval  $T_s = 25\mu s$

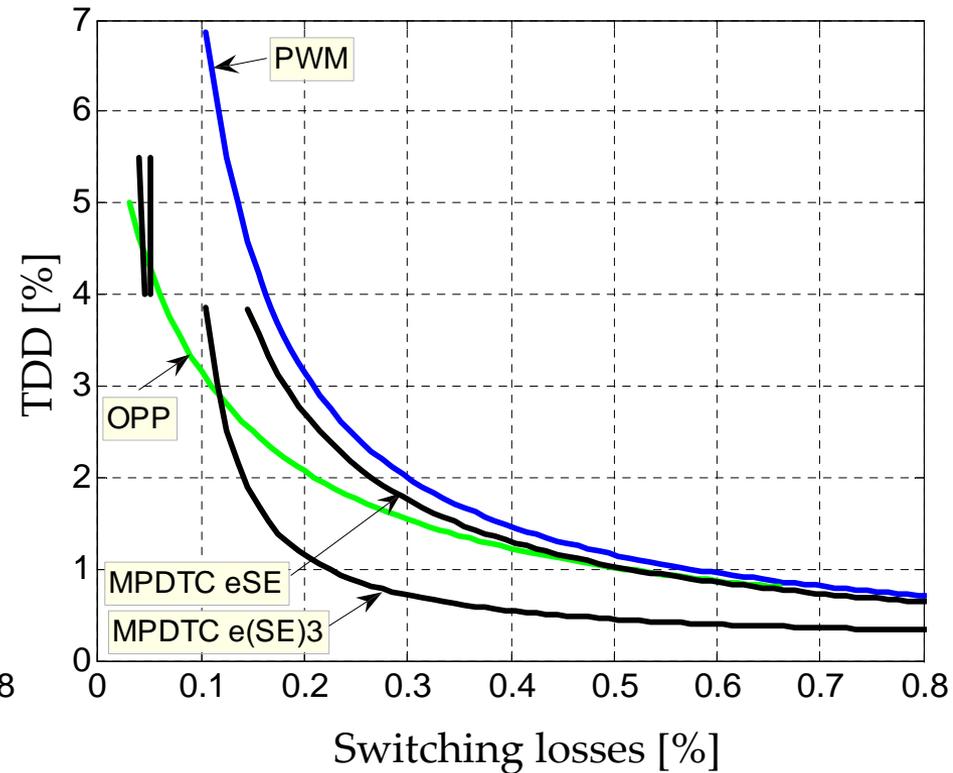


# Model Predictive Direct *Torque* Control

## Current TDD vs switching losses



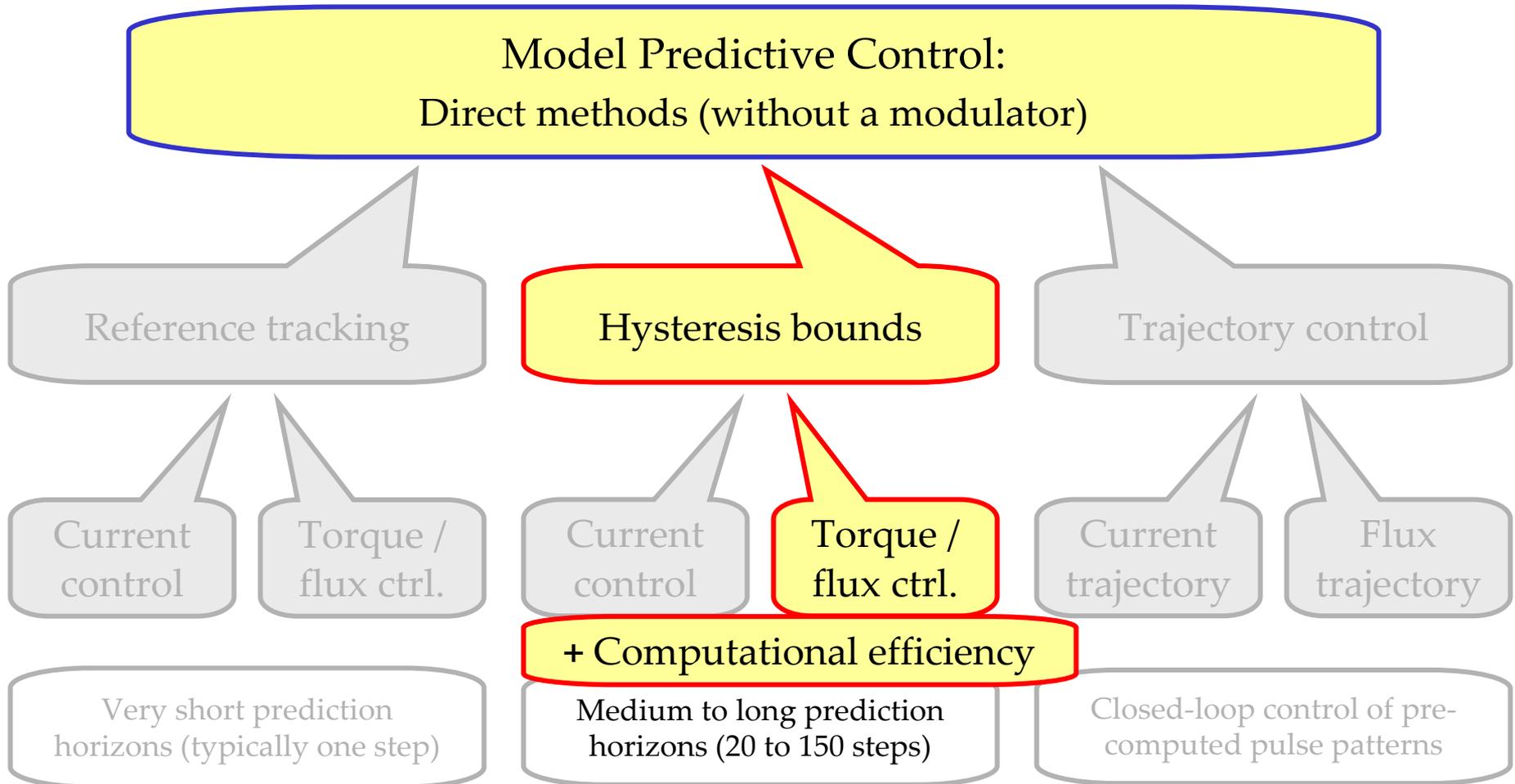
## Torque TDD vs switching losses



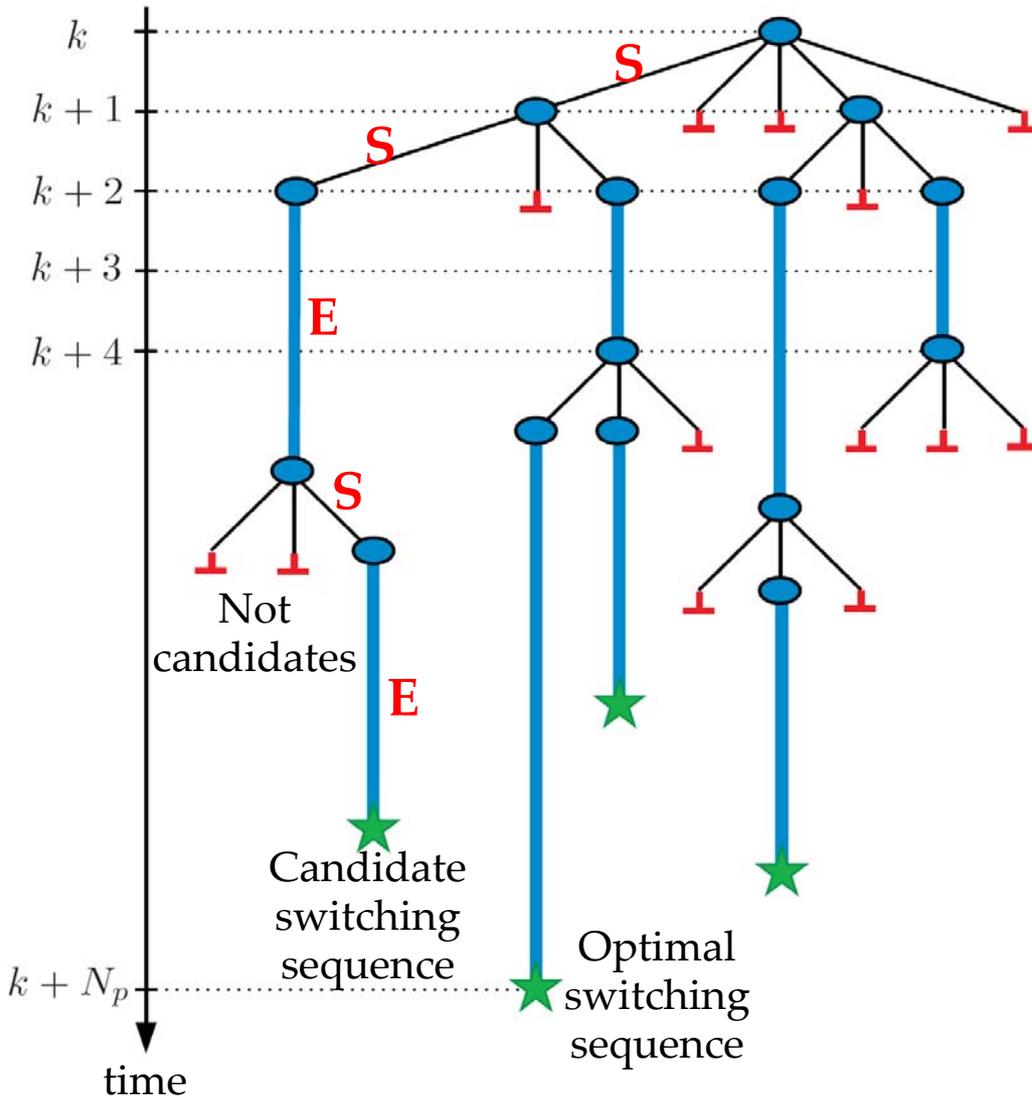
Long switching horizon eSESESE (50-150 steps):

- Current THD: similar to optimized pulse patterns (OPP)
- Torque THD: significantly better than OPP, but at the expense of current THD – points on curves do **not** correspond to each other!

# Classification of MPC Schemes for Electrical Drives



# Search Tree

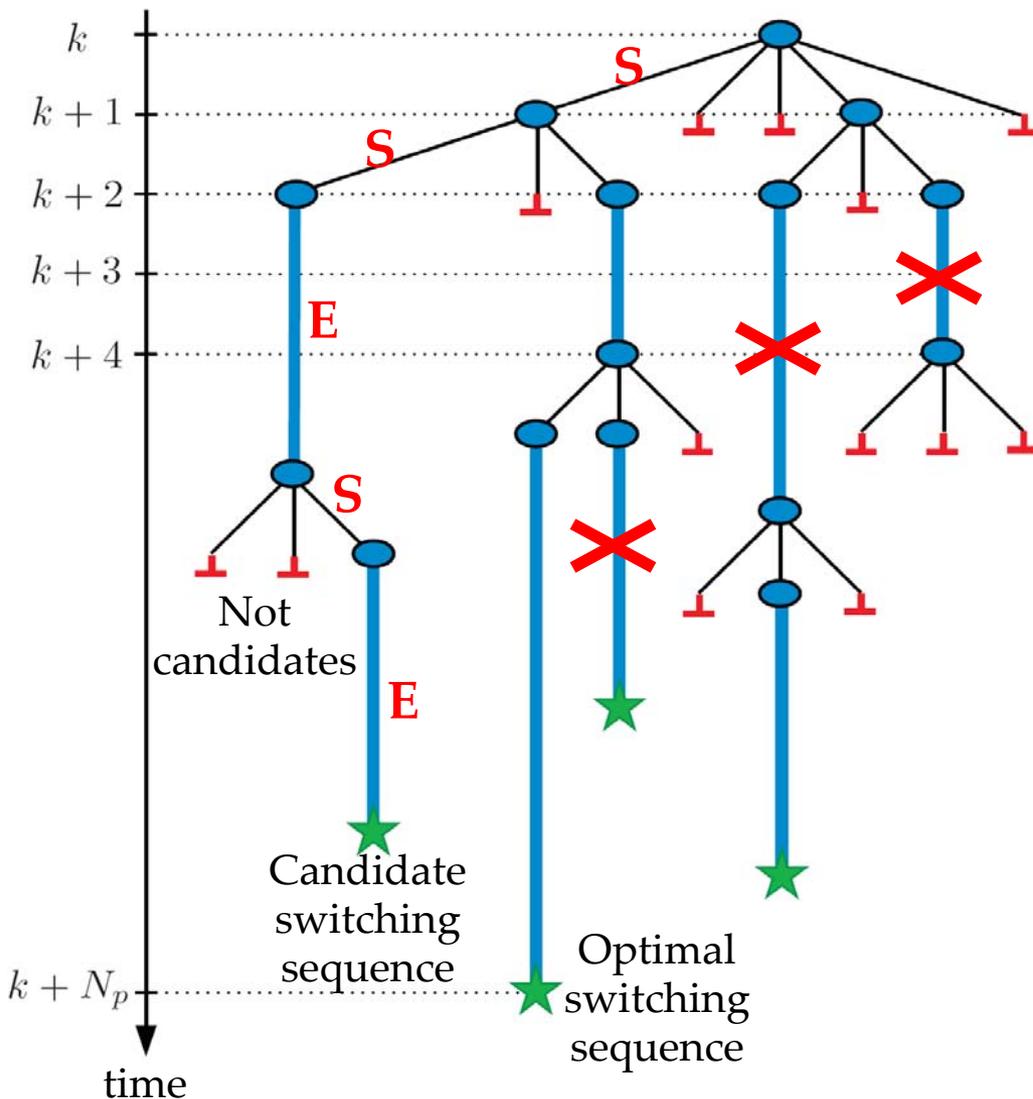


Search tree induced by optimization problem

Computational burden  $\approx$  number of nodes

So far: full enumeration

# Search Tree



Search tree induced by optimization problem

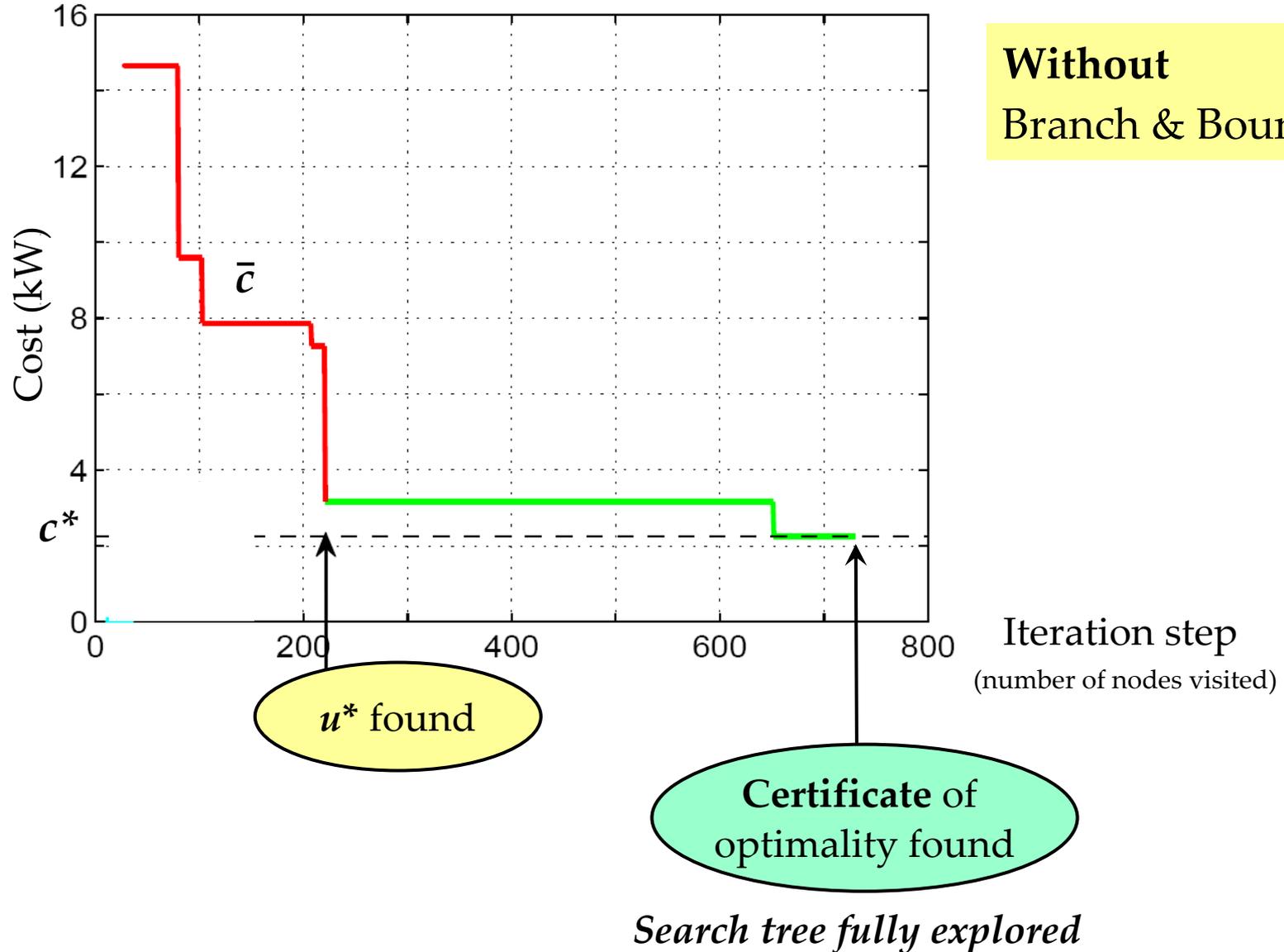
Computational burden  $\approx$  number of nodes

So far: full enumeration

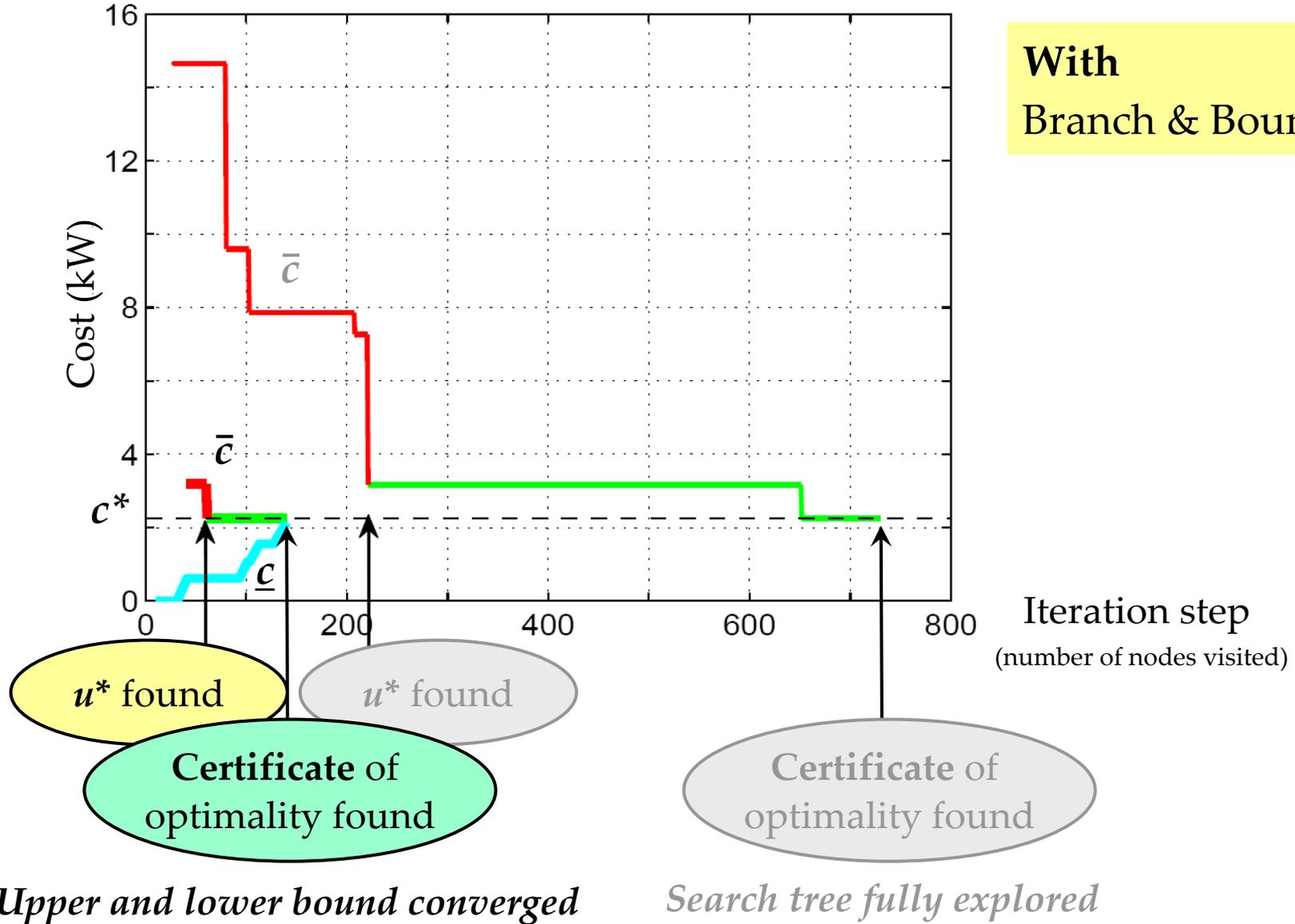
Approaches to reduce computation time?

- More efficient **implementation** of algorithm
- More efficient **extension** / extrapolation step
- Reduce number of nodes explored in search tree by using **Branch & Bound**

# Evolution of the Optimal Cost during Optimization



# Evolution of the Optimal Cost during Optimization

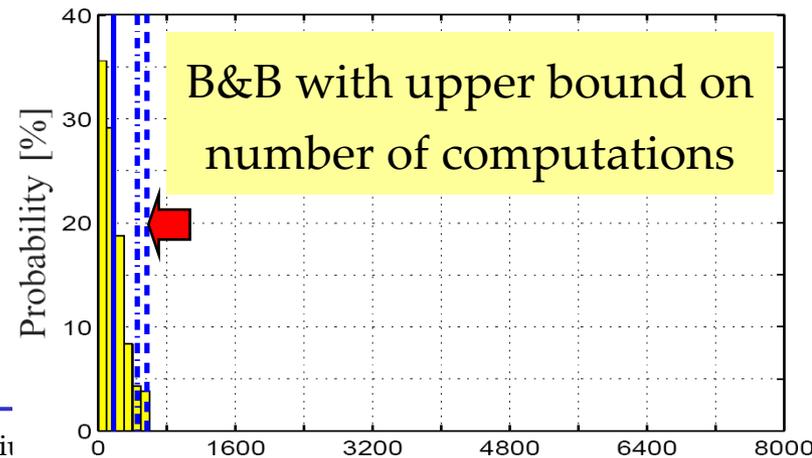
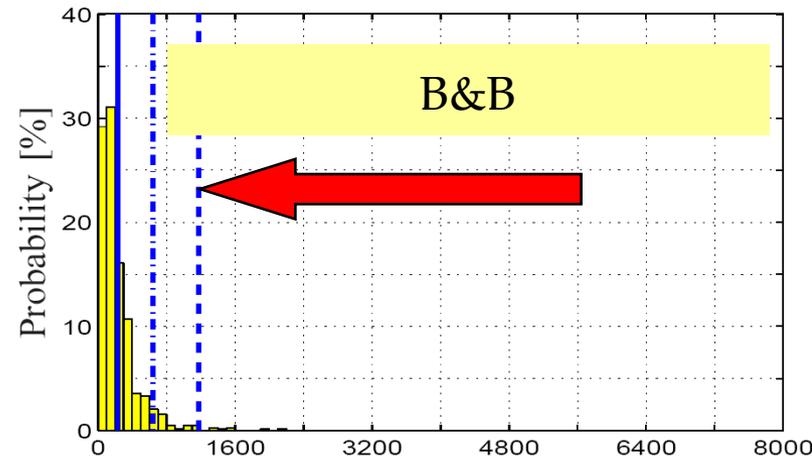
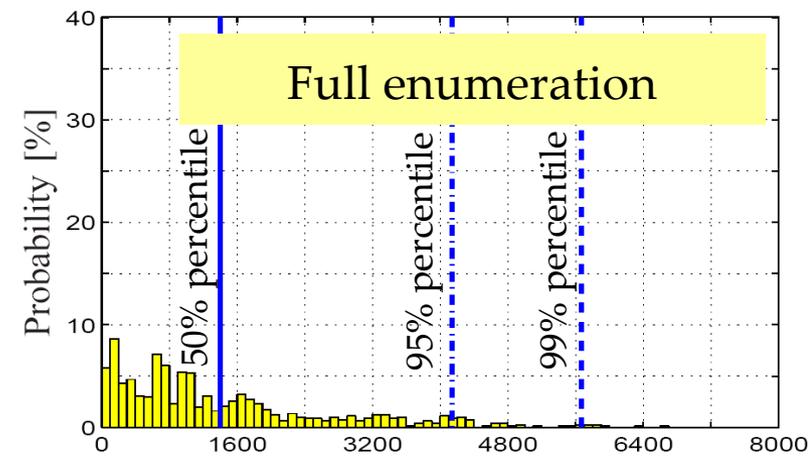


# Computational Effort

**Example:** MPDTC with the switching horizon 'eSSESESE'

**Probability distributions:**

**Number of nodes** required to be explored to obtain the **optimal cost  $c^*$**



# Performance vs Computational Burden

Controller settings			Pred. horizon		Nodes explored		$u^*$	Performance [%]			
Sw. horizon	$N_{\max}$	$j_{\max}$	avg.	max.	avg.	max.	found [%]	$P_{\text{sw}}$	$f_{\text{sw}}$	$I_{s,\text{THD}}$	$T_{e,\text{THD}}$
DTC	–	–	–	–	–	–	–	100	100	100	100
eSSE	–	–	26.6	96	112	277	100	57.3	71.2	103	98.4
eSSE	50	50	22.0	97	43.6	50	92.2	58.3	74.1	104	103
eSSESESE	–	–	98.2	150	3246	7693	100	37.9	48.9	97.0	92.0
eSSESESE	110	600	88.0	152	483	600	92.1	38.6	51.4	97.3	94.0

## Short switching horizon (eSSE):

- B&B => computational burden reduced by **factor 5.5**
- Switching losses and THDs merely affected

**Benefit: simplify** implementation for **short** switching horizons

# Performance vs Computational Burden

Controller settings			Pred. horizon		Nodes explored		$u^*$	Performance [%]			
Sw. horizon	$N_{\max}$	$j_{\max}$	avg.	max.	avg.	max.	found [%]	$P_{\text{sw}}$	$f_{\text{sw}}$	$I_{s,\text{THD}}$	$T_{e,\text{THD}}$
DTC	–	–	–	–	–	–	–	100	100	100	100
eSSE	–	–	26.6	96	112	277	100	57.3	71.2	103	98.4
eSSE	50	50	22.0	97	43.6	50	92.2	58.3	74.1	104	103
eSSESESE	–	–	98.2	150	3246	7693	100	37.9	48.9	97.0	92.0
eSSESESE	110	600	88.0	152	483	600	92.1	38.6	51.4	97.3	94.0

## Short switching horizon (eSSE):

- B&B => computational burden reduced by factor 5.5
- Switching losses and THDs merely affected

Benefit: simplify implementation for short switching horizons

## Long switching horizon (eSSESESE):

- B&B => computational burden reduced by factor 13
- Switching losses and THDs merely affected

Benefit: enable implementation for long switching horizons

# Performance Results

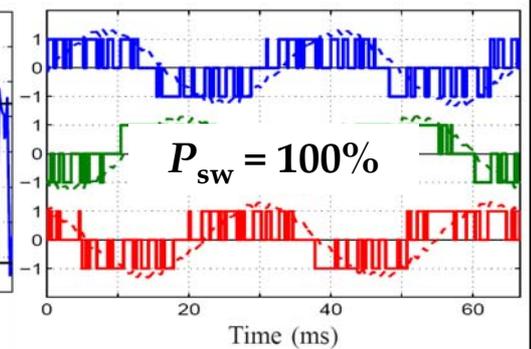
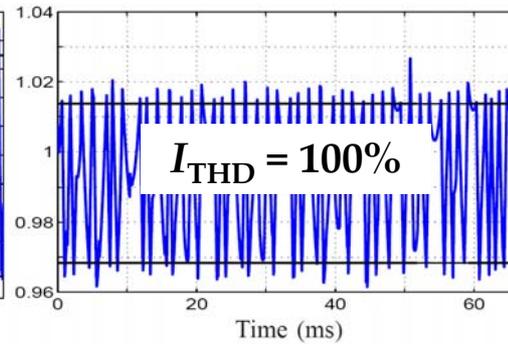
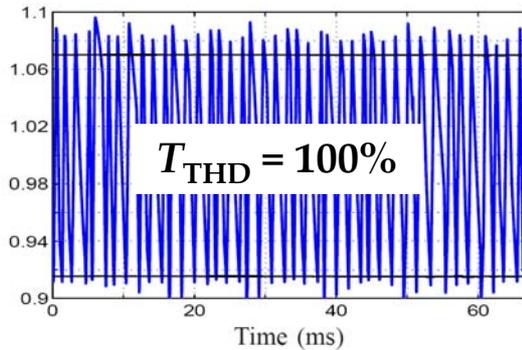
ACS 6000,  $w_e=0.6$  pu,  $T_e=1$  pu;  
Same torque bounds, flux bounds relaxed by +/- 0.01pu  
ABB's simulation environment

Torque

Stator flux

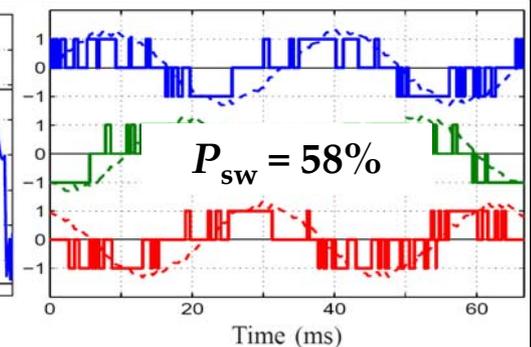
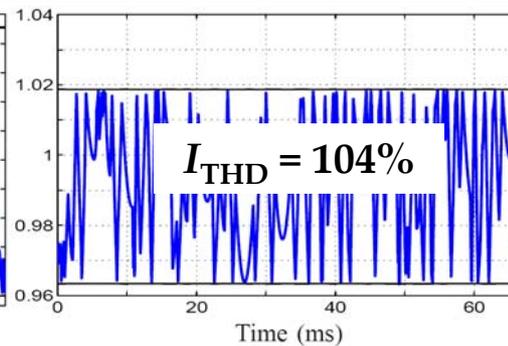
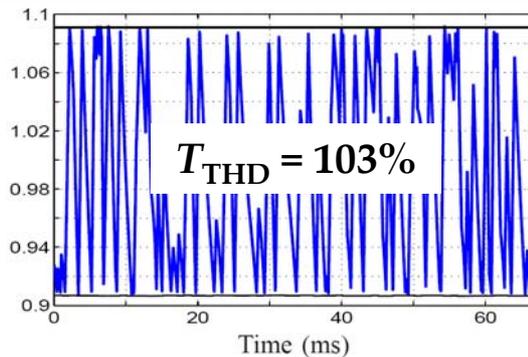
Switch positions

Standard  
DTC



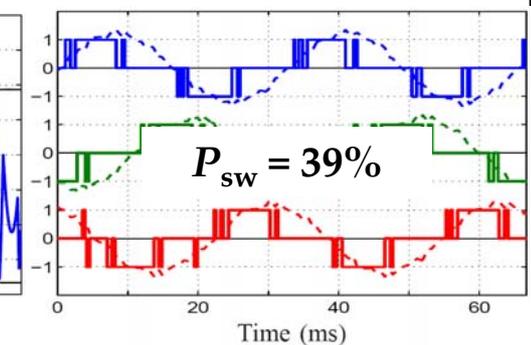
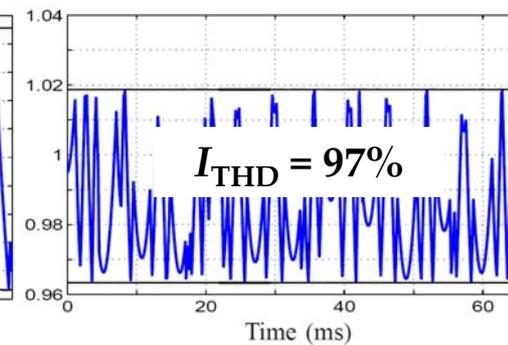
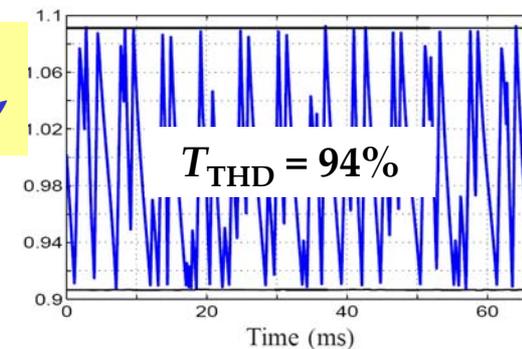
MPDTC  
'eSSE'

$N_p = 22$



MPDTC  
'eSSE(SE)<sup>2</sup>'

$N_p = 88$



# Summary and Conclusions

# Commercial Benefits

- Higher **rating** of inverter possible
  - 40% higher power capability (e.g. from 5 MVA to 7 MVA)
  - Hardware remains the same
- **Standard machines** can be used
  - **No derating** of machine required
- For '**complicated**' topologies
  - MPC is **enabling** technology



**Fully utilize the drive hardware**

# Summary and Conclusions

---

**Goal:** Fully utilize *capability* of drive hardware

- Minimize **switching losses** per **distortions**
- Achieve very **fast** torque and current response

**Approach:**

- Treat control and modulation problem in **one stage**
- Work in the **time-domain**
- Adopt **model predictive control**

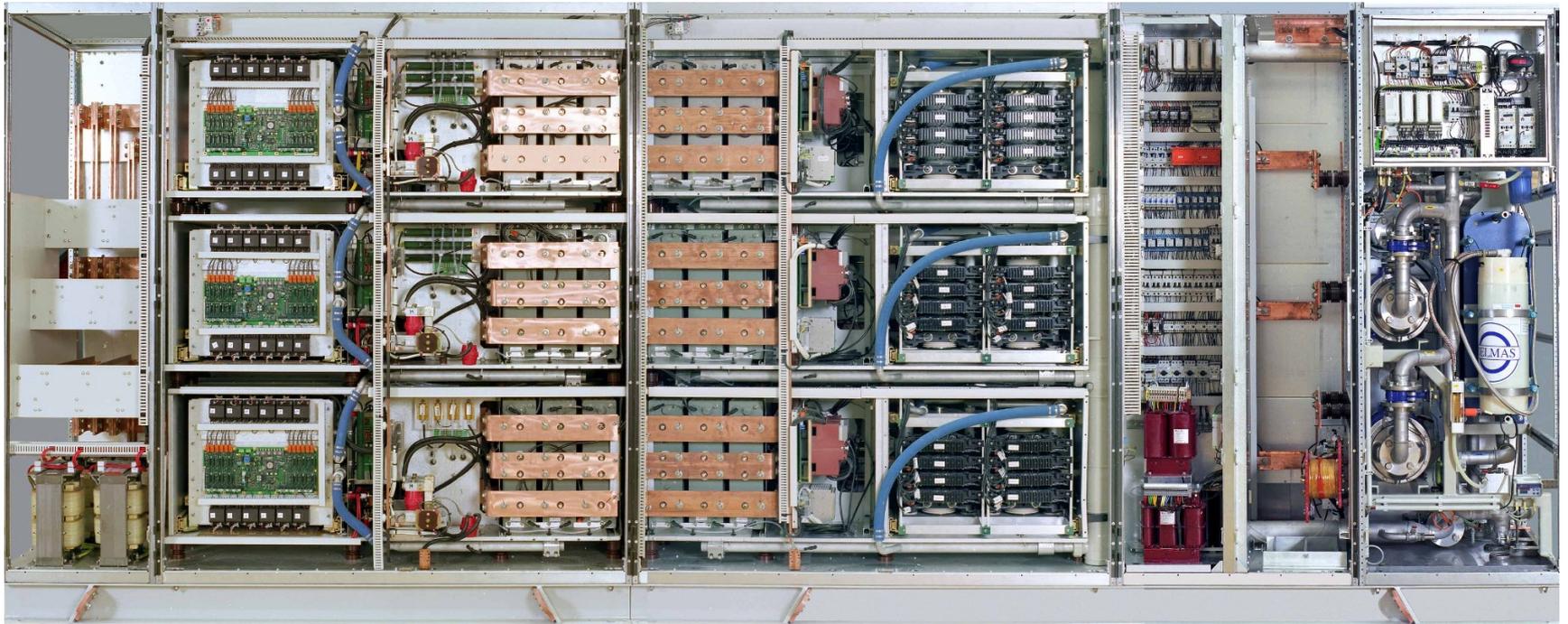
**Results:**

- MPDxC family
- MP<sup>3</sup>C

# For More Information

---

[www.ece.auckland.ac.nz/tgey001](http://www.ece.auckland.ac.nz/tgey001)



# Selected Literature

---

- T. Geyer: "Low complexity model predictive control in power electronics and power systems", PhD thesis, Automatic Control Laboratory, ETH Zurich, Switzerland, Mar. 2005.
- P. Cortés, M. P. Kazmierkowski, R. M. Kennel, D. E. Quevedo, and J. Rodríguez: "Predictive Control in Power Electronics and Drives", IEEE Trans. on Industrial Electronics, vol. 55, no. 12, pp. 4312-4324, Dec. 2008.
- T. Geyer, G. Papafotiou, and M. Morari: "Model predictive direct torque control - part I: concept, algorithm and analysis", IEEE Trans. on Industrial Electronics, vol. 56, no. 6, pp. 1894-1905, June 2009.
- G. Papafotiou, J. Kley, K. Papadopoulos, P. Bohren, M. Morari: "Model predictive direct torque control - part II: implementation and experimental evaluation", IEEE Trans. on Industrial Electronics, vol. 56, no. 6, pp. 1906-1915, June 2009.
- T. Geyer: "Generalized model predictive direct torque control: long prediction horizons and minimization of switching losses", Proc. of the 48rd IEEE Conference on Decision and Control, Shanghai, China, Dec. 2009.
- T. Geyer: "A comparison of control and modulation schemes for medium-voltage drives: emerging predictive control concepts versus field oriented control", Proc. of the Energy Conversion Congress and Exposition, Atlanta, GA, Sep. 2010.
- T. Geyer: "Model predictive direct current control for multi-level converters", Proc. of the Energy Conversion Congress and Exposition, Atlanta, GA, Sep. 2010.