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# Applying Simple Data-Driven Control Algorithms In Low-Voltage Grids With Flexibility Provided By Electric Vehicles For Grid-Oriented Control

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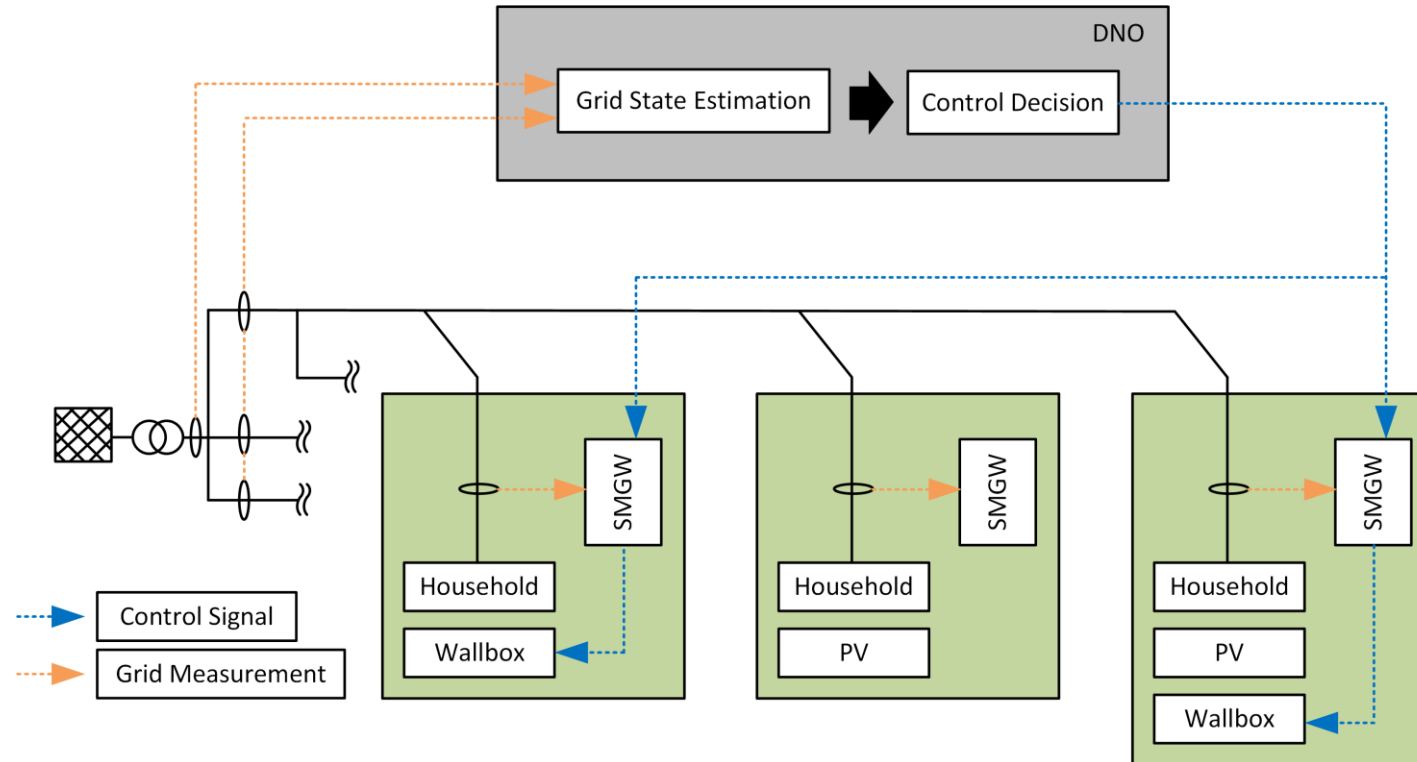
## Agenda

- 1) Motivation
- 2) Problem Formulation
- 3) Methode
- 4) Test Scenario
- 5) Simulation Result
- 6) Conclusion

**Development:** The number of electric vehicles (EVs) is increasing rapidly

**Potential Issue:** Charging processes of EVs can lead to grid congestion

**Available Solution:** Distribution system operators (DSOs) are allowed to reduce EV charging power if critical grid states are identified



1. Real-time measurement data is limited
2. Grid models in low-voltage (LV) grids are not exact

### Requirements for the grid-oriented control in LV grids in this paper:

#### Data Availability

No access to smart meters, rather grid states measured at transformer-level

#### Model Accuracy

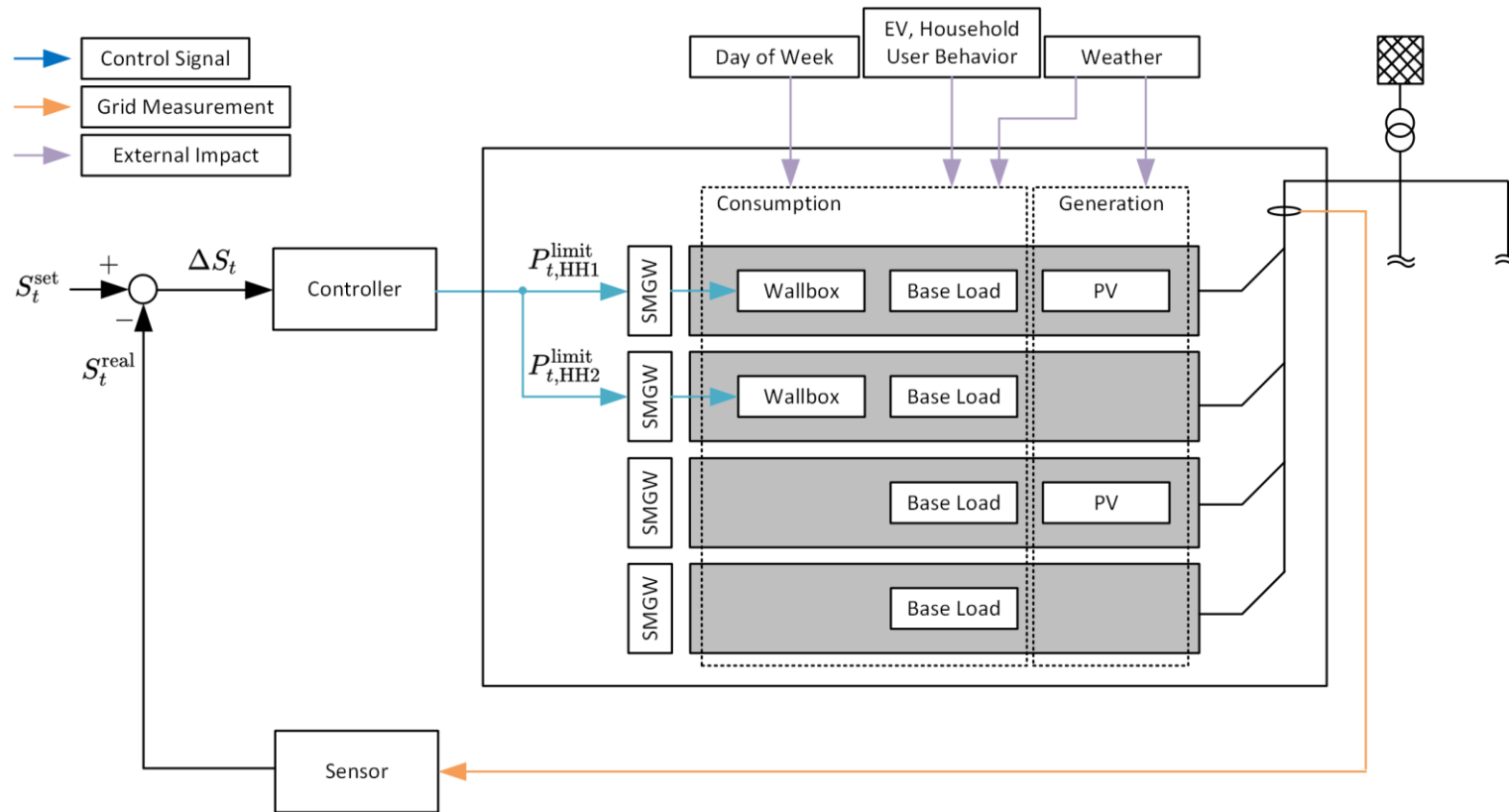
No grid model is needed for decision-making in the control process

#### System Complexity

Control algorithm contains few parameters and uses only online data

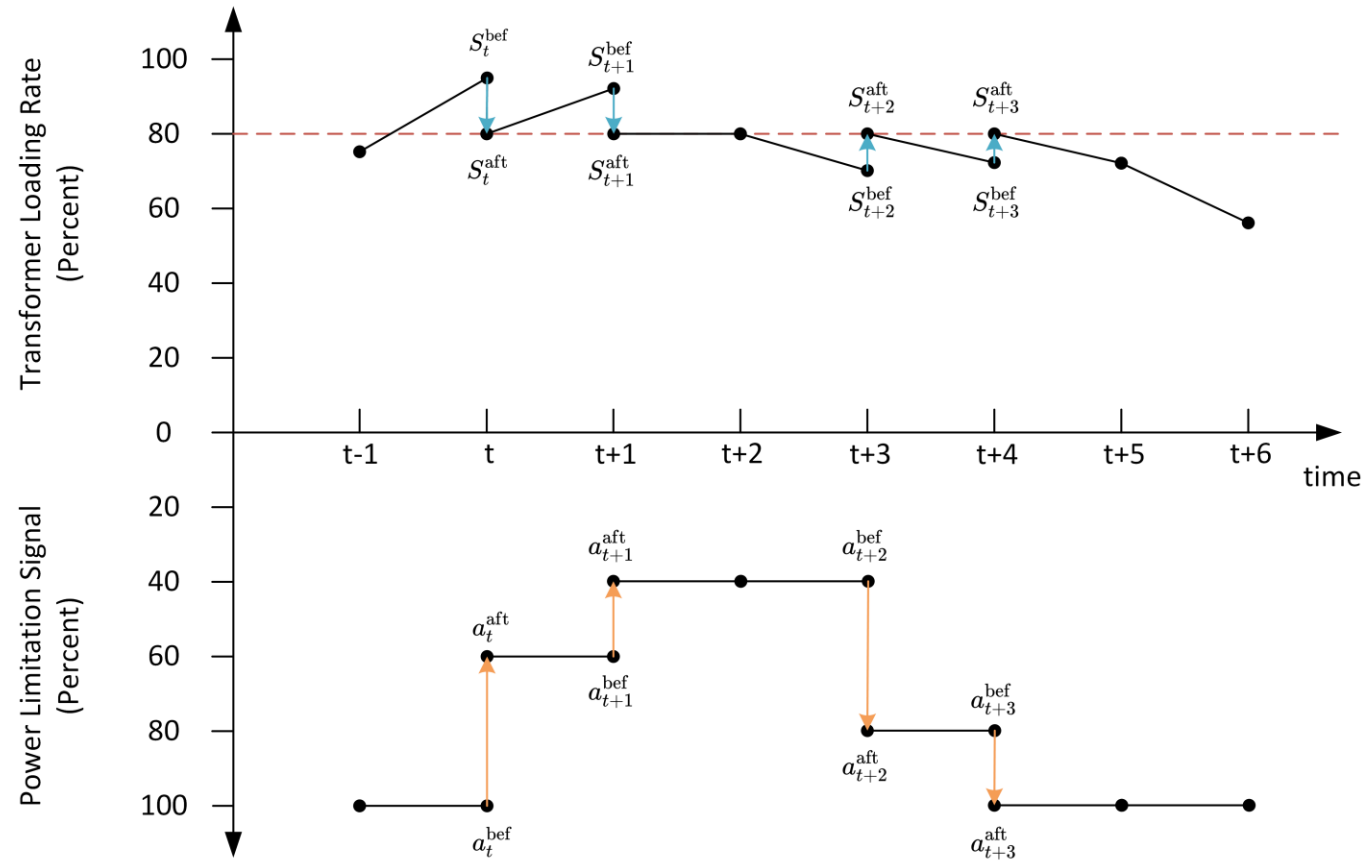
### Research question of this work:

What is the performance of a simple data-driven control method based on online algorithms using limited real-time measurement data in the grid-oriented control?



The objective of the controller is to find the solution of this optimization problem:

$$a_t^* = \arg \min_{a_t} |S_t^{\text{set}} - S_t^{\text{real}}| \quad \text{with} \quad P_{t,HH i}^{\text{limit}} = a_t * P_{HH i}^{\text{install}} \quad \forall i \in W$$



The most important relationship that needs to be estimated is:

$$S_t^{\text{aft}} - S_t^{\text{bef}} = f(a_t^{\text{aft}} - a_t^{\text{bef}})$$

### Basic idea of the control algorithm:

Model-Free Adaptive Control (MFAC): build a dynamic linearization model using input and output from controlled plant without knowledge about system models and system states

Step 1: estimate the pseudo partial derivative

$$\hat{\phi}_t = \hat{\phi}_{t-1} + \frac{\eta \Delta a_{t-1}}{\mu + \Delta a_{t-1}^2} (\Delta S_{t-1} - \hat{\phi}_{t-1} \Delta a_{t-1})$$

Step 2: calculate needed control decision

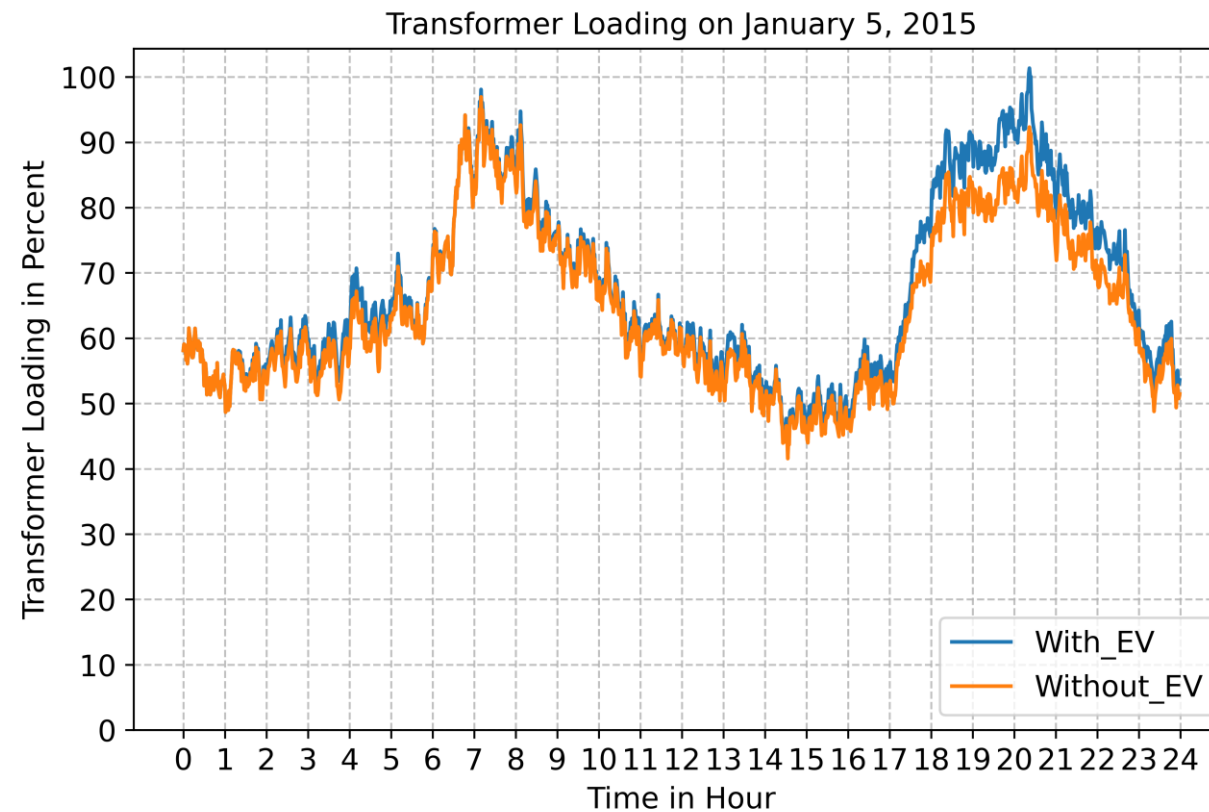
$$a_t^{\text{aft}} = a_t^{\text{bef}} + \frac{\rho \hat{\phi}_t}{\lambda + \hat{\phi}_t^2} (S_t^{\text{set}} - S_t^{\text{bef}})$$

### Reference LV grid model from SimBench

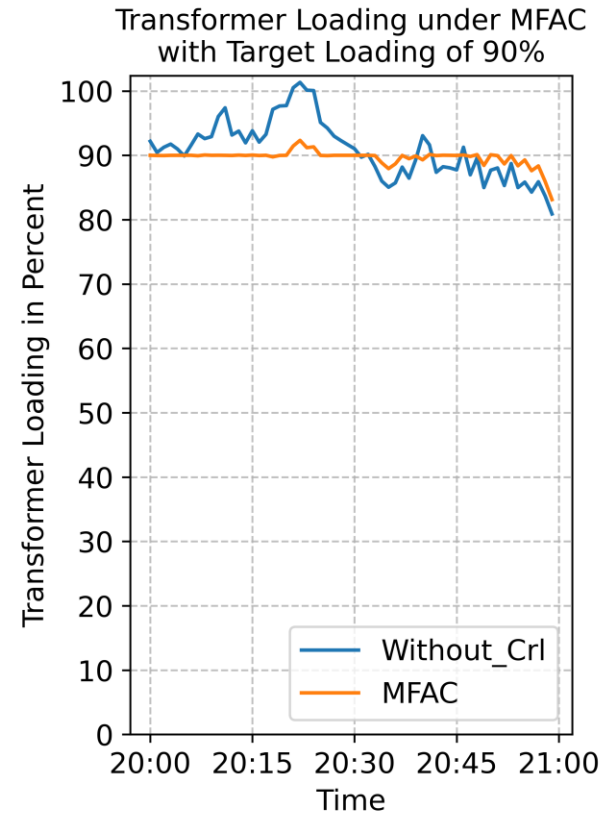
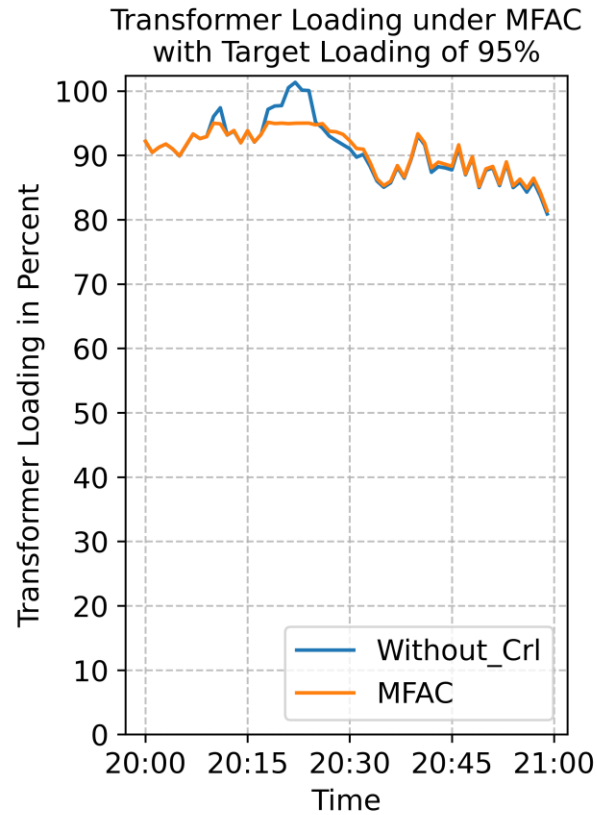
- One MV/LV transformer
- 7 LV feeder lines
- Radial structure
- Germany

### Load profiles of households from Pecan Street

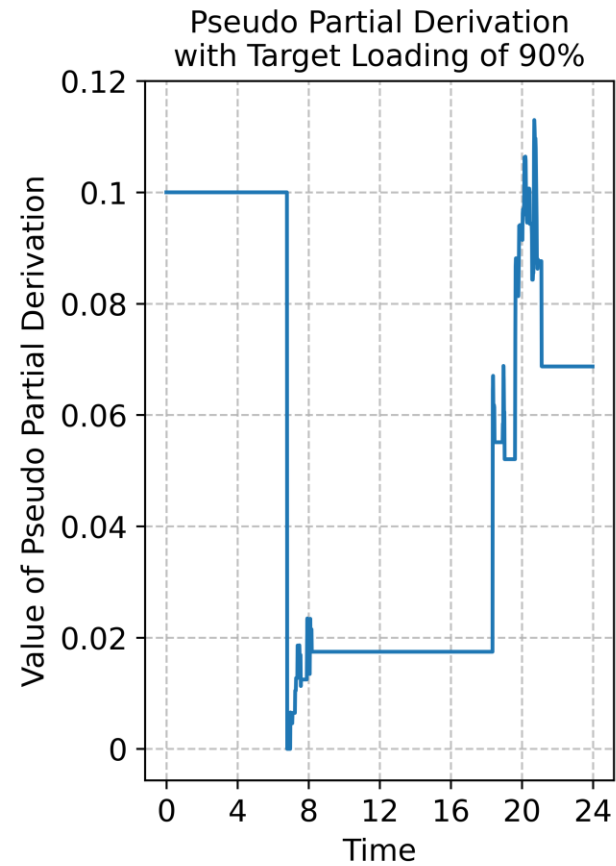
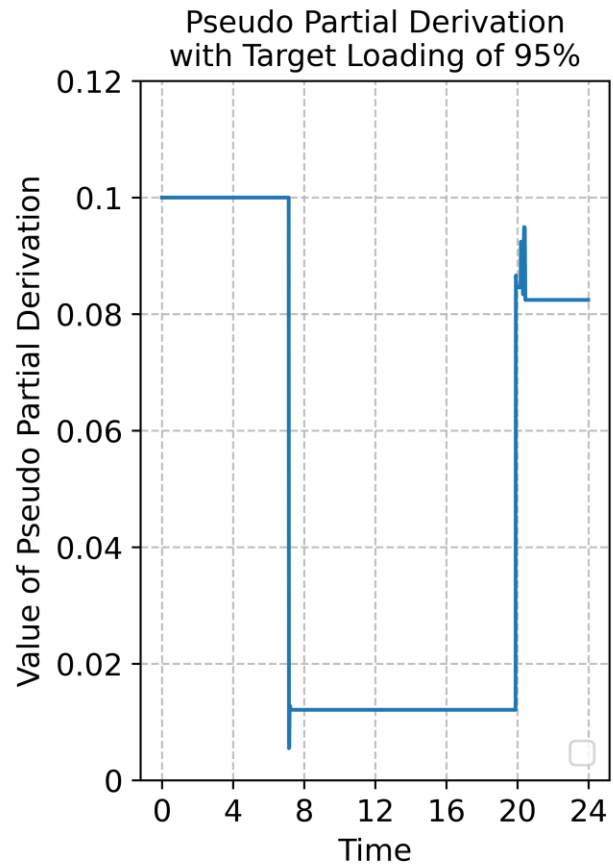
- 350 Households
- 54 private EV charging points
- 10 PV panels
- Texas USA



1. Two peak loads are observed at about 7:30 and 20:30
2. Maximum loading rate of transformer has reached 100%



| Target transformer loading | Number of time steps with overloads | Mean transformer loading during overloads |
|----------------------------|-------------------------------------|---|
| 95%                        | 1                                   | 95.14%                                    |
| 90%                        | 12                                  | 90.57%                                    |



| Parameter      | Value         |
|----------------|---------------|
| $\eta$         | 1.0           |
| $\mu$          | $1 * 10^{-6}$ |
| $\rho$         | 1.0           |
| $\lambda$      | $1 * 10^{-6}$ |
| $\hat{\phi}_0$ | 0.1           |

### **Answer to the research question:**

- MFAC control algorithm can successfully relieve the overloads of transformer without knowledge about real-time states of EVs and exact grid models
- Pseudo partial derivative with only one parameter that needs to be estimated can extract and follow the frequent change of system dynamic in LV grids
- Mean control error regarding transformer loading during the overload period is less than 1%

### **Future work:**

- Other forms of MFAC algorithm can be tested
- Find out the impact of hyperparameters on control performance

**Thanks for your attention!**